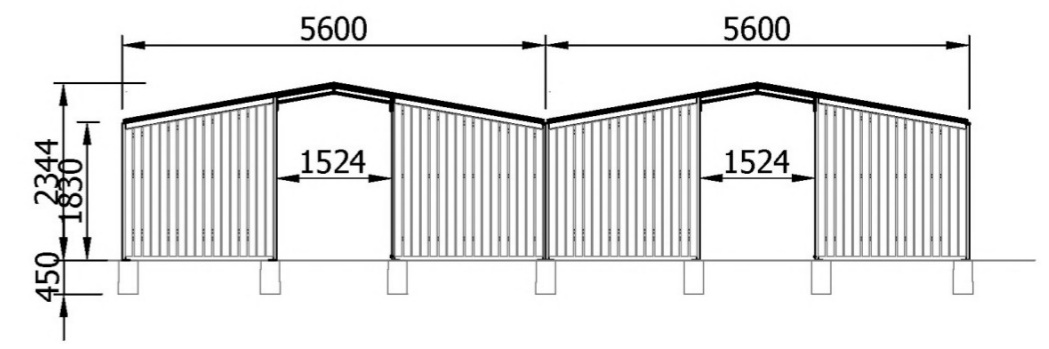
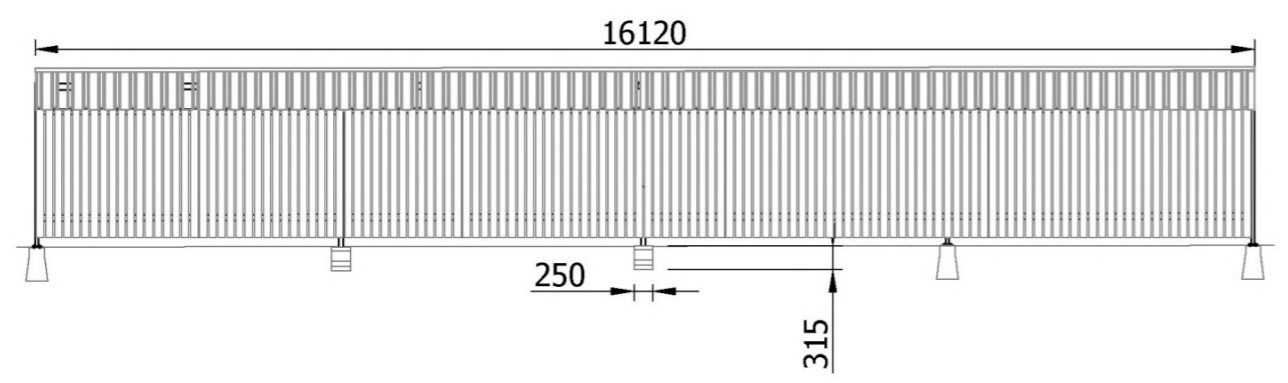
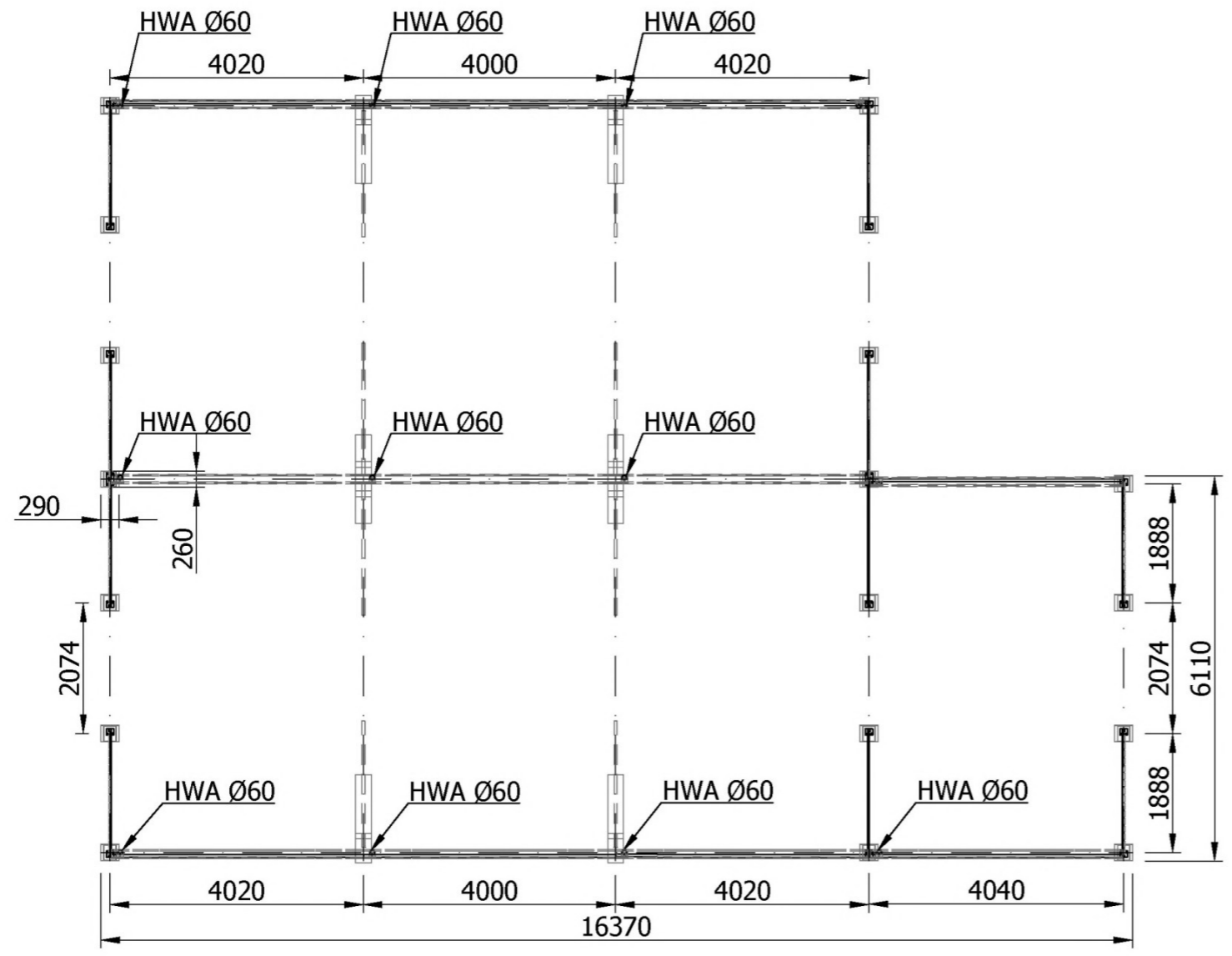



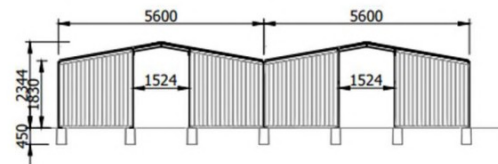
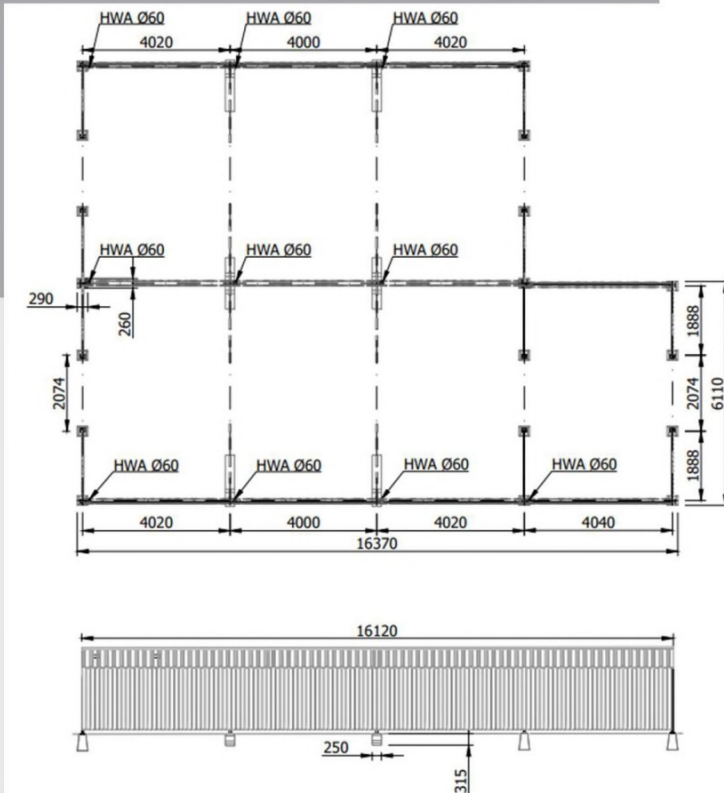
| Rev | Datum | Door |
|-----|-----------|------|
| - | 13-4-2023 | |



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STATIC CALCULATION

Tel-C 2x3+4-vaks



CONSTRUCTOR | [REDACTED]

DATE | 20-4-2023

REFERENCE | 00.821.996

Project 129958
Reference 00.821.996
Date 20-4-2023

Client

Constructor



Terms and conditions

This static calculation has been carried out in accordance with the “Legal relationship client-architect, engineer and consultant” DNR 2011 (Dutch version) and the General Terms and Conditions (Dutch version) of Falco BV. By accepting this calculation, you declare that you have taken note of the contents of the above conditions.

Responsibility for these calculations and drawings rests solely with Falco BV.

This calculation serves as a starting point for the calculation of the prefab components or detailed calculations and detailing of steel structures. And is fully based on the applicable norm sheets and National Annexes.

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3.0 Load combinations

3.1 Ultimate Limit State

| | | |
|---------------|------------|--|
| Fundamental B | exp. 6.10a | $0,9 G_k + 1,5 \psi_{0;1} Q_{k;1} + 1,5 \psi_{0;j} Q_{k;j}$ |
| | | $1,35 G_k + 1,5 \psi_{0;1} Q_{k;1} + 1,5 \psi_{0;j} Q_{k;j}$ |
| | exp. 6.10b | $0,9 G_k + 1,5 Q_{k;1} + 1,5 \psi_{0;j} Q_{k;j}$ |
| | | $1,2 G_k + 1,5 Q_{k;1} + 1,5 \psi_{0;j} Q_{k;j}$ |

3.2 Serviceability Limit State

| | | |
|------------------|------------|---|
| Characterization | exp. 6.14b | $1,0 G_k + 1,0 Q_{k;1} + 1,0 \psi_{0;j} Q_{k;j}$ |
| Frequent | exp. 6.15b | $1,0 G_k + 1,0 \psi_{1;1} Q_{k;1} + 1,0 \psi_{2;j} Q_{k;j}$ |
| Quasi-permanent | exp. 6.16b | $1,0 G_k + 1,0 \psi_{2;j} Q_{k;j}$ |

4.0 Loads

4.1 Location

| | | |
|-----------|-----------|-----------------|
| Street | | Volmolenweg |
| ZIP Code | | 6961 VN |
| City | | Eerbeek |
| Country | | The Netherlands |
| Latitude | ϕ | = 52.101 ° |
| Longitude | λ | = 6.063 ° |
| Altitude | A | = 14 m |

4.2 Dead loads

| | | | | |
|------------------------------------|-------|---|-------|-------------------|
| Roof steel plate VD35R/1035 0,75mm | G_k | = | 0,095 | kN/m ² |
|------------------------------------|-------|---|-------|-------------------|

4.3 Snow loads

| | | | | |
|-------------------------|------------|---|------|-------------------|
| Snow zone N° | | = | 1 | |
| Exposure coefficient | C_e | = | 1,00 | |
| Thermal coefficient | C_t | = | 1,00 | |
| Snow load on the ground | S_k | = | 0,70 | kN/m ² |
| Pitch of roof | α_1 | = | 0,00 | ° |
| Shape coefficient | μ_1 | = | 0,80 | |
| Snow calculation value | s | = | 0,56 | kN/m ² |



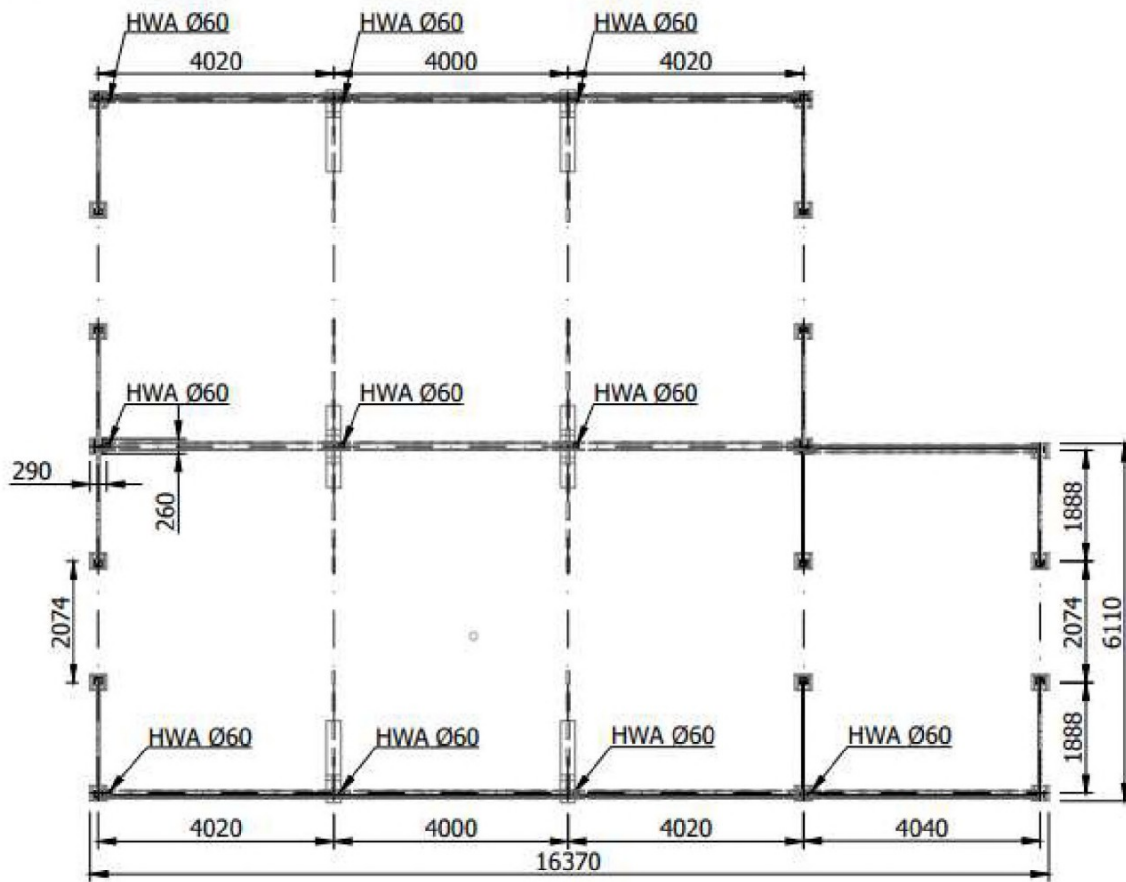
4.4 Wind loads

| | | | | |
|---------------------------------|--------------|---|--------|-------------------|
| Wind zone N° | | = | III | |
| Shelter height | z | = | 2,344 | m |
| Shelter width | d | = | 11,200 | m |
| Shelter length | l | = | 16,120 | m |
| Directional factor | C_{dir} | = | 1,000 | |
| Seasonal factor | C_{season} | = | 1,000 | |
| Structural factor | $C_s C_d$ | = | 1,000 | |
| Shape parameter | K | = | 0,200 | |
| Turbulence factor | K_t | = | 1,000 | |
| Fundamental value wind velocity | $v_{b,0}$ | = | 24,500 | m/s |
| Basic wind velocity | V_b | = | 24,500 | m/s |
| Basic velocity pressure | Q_b | = | 0,380 | kN/m ² |
| Topography coefficient | $C_o(z)$ | = | 1,000 | |
| Terrain category | | = | III | |
| Peak velocity pressure | $q_p(z)$ | = | 0,476 | kN/m ² |

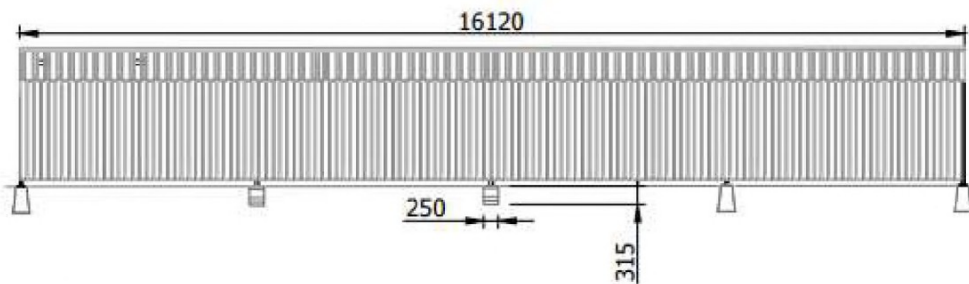


5.0 Static calculation cycle shelter

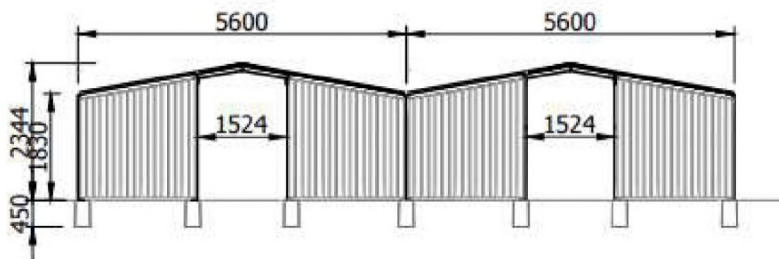
5.1 Overview



Ground floor plan



Side elevation



Front elevation

5.2 Calculation

Construction

The shelter is calculated in Autodesk Robot.

| | | |
|------------|-------|------------------------|
| Load cases | DL1 | Dead load construction |
| | | Dead load roof sheets |
| | SN1 | Snow load |
| | WIND1 | Wind loads X+ |
| | WIND2 | Wind loads Y+ |
| | WIND3 | Wind loads X- |
| | WIND4 | Wind loads Y- |

For calculation and verification see "6.0 Output Autodesk Robot calculation"

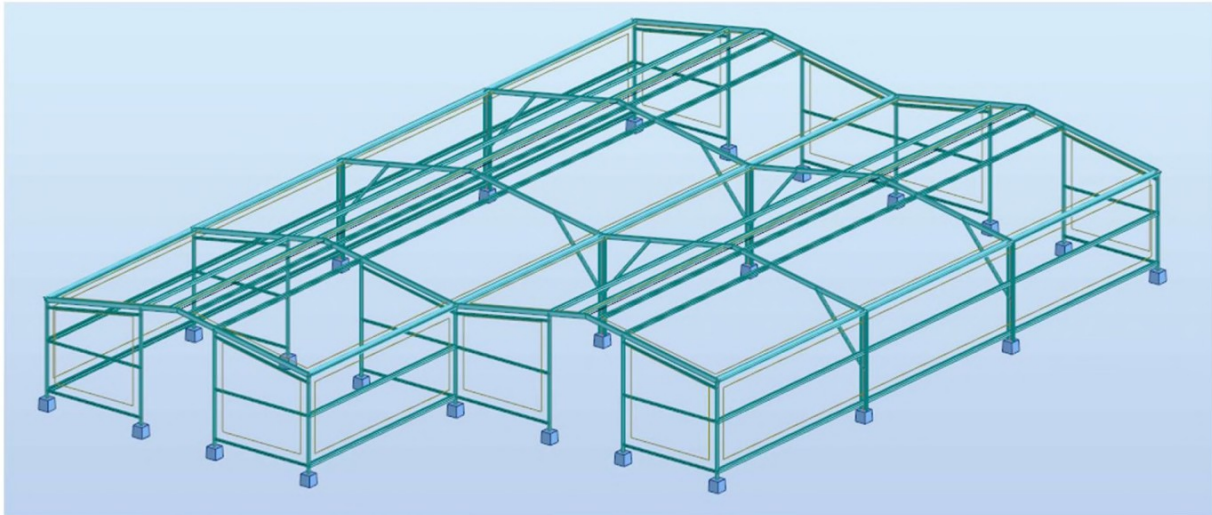


Figure of shelter built in Robot

6.0 Output Autodesk Robot calculation

6.1 Structure view

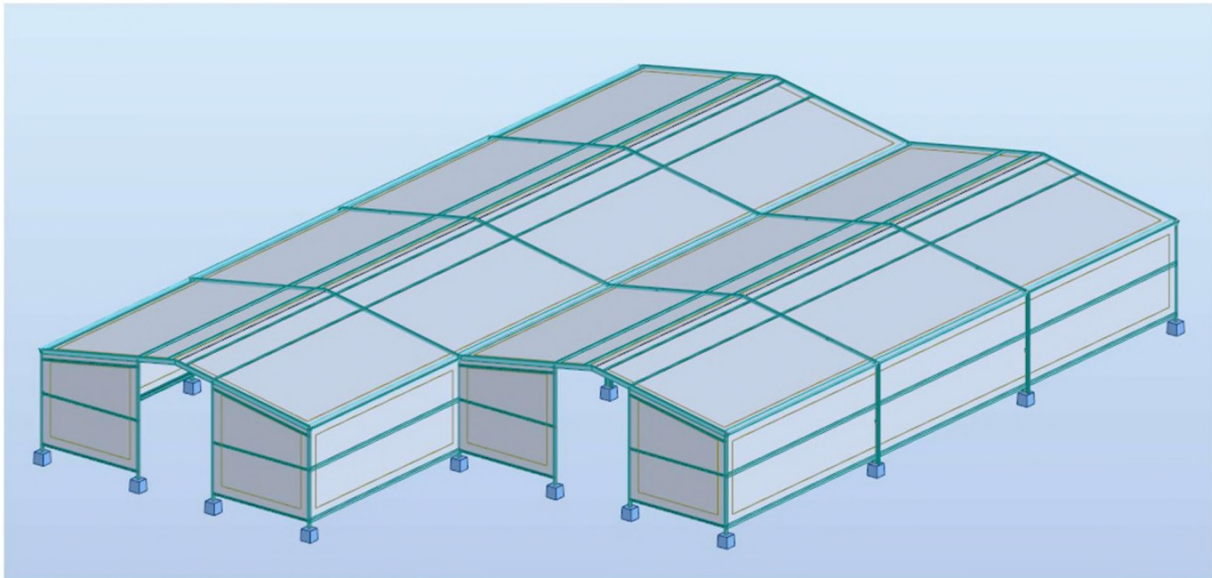


Figure of structure with claddings

6.2 Data – Materials

| | Material | E (MPa) | G (MPa) | NI | LX (1/°C) | RO (kN/m3) | Re (MPa) |
|---|----------|-----------|----------|------|-----------|------------|----------|
| 1 | S235 | 210000,00 | 80800,00 | 0,30 | 0,00 | 77,01 | 235,00 |

6.3 Data – Sections

| Section name | Member list | AX (cm2) | AY (cm2) | AZ (cm2) | IX (cm4) | IY (cm4) | IZ (cm4) |
|---------------|---------------------|----------|----------|----------|----------|----------|----------|
| K 40x20x2 | 25to54 | 2,24 | 0,80 | 1,60 | 3,34 | 4,45 | 1,44 |
| TELG 80x40x3 | 81to124 | 4,53 | 2,17 | 2,33 | 0,14 | 44,29 | 7,06 |
| TELG 100x65x3 | 125to135 | 8,77 | 4,11 | 3,77 | 0,28 | 205,75 | 54,43 |
| IPE 120 | 12to17 | 13,21 | 8,06 | 5,28 | 1,69 | 318,00 | 27,67 |
| K 40x40x2 | 1to11 18to24 73to80 | 3,04 | 1,60 | 1,60 | 10,97 | 7,34 | 7,34 |
| K 80x40x3 | 55to64 | 6,84 | 2,40 | 4,80 | 42,72 | 55,85 | 18,43 |
| K 70x50x4 | 65to72 | 8,96 | 4,00 | 5,60 | 65,84 | 59,50 | 34,64 |

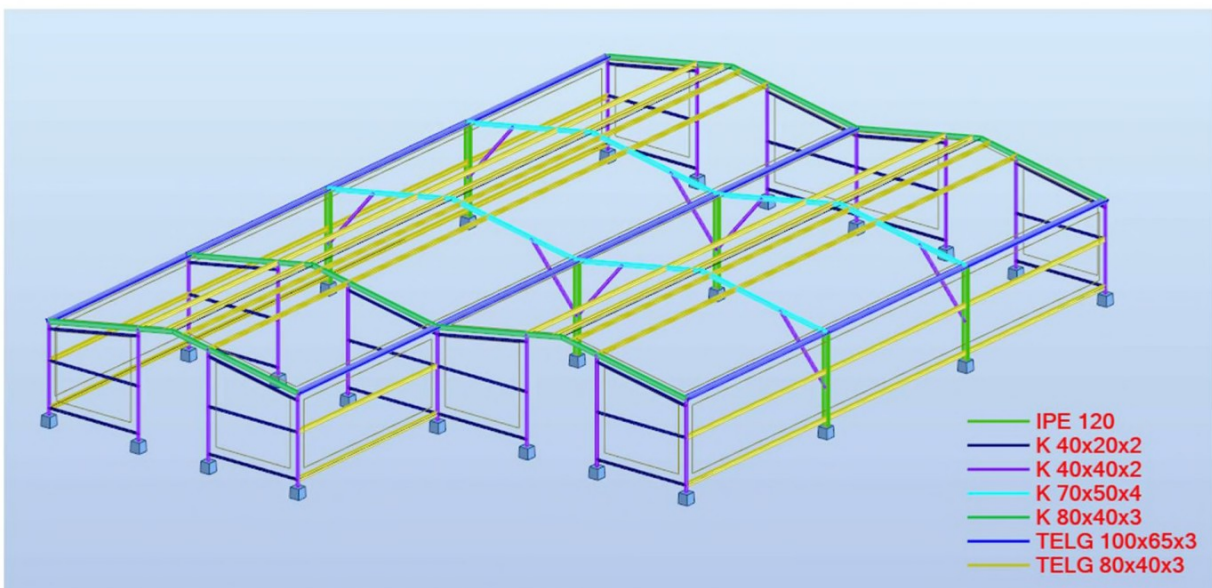


Figure of structure with marked sections

6.4 Section properties

K 40x20x2



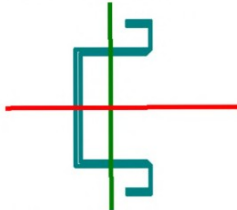
HY=2,0, HZ=4,0 [cm]
 AX=2,24 [cm²]
 IX=3,34, IY=4,45, IZ=1,44 [cm⁴]
 Material=S235

TELG 80x40x3



HY=4,0, HZ=8,0 [cm]
 AX=4,53 [cm²]
 IX=0,14, IY=44,29, IZ=7,06 [cm⁴]
 Material=S235

TELG 100x65x3



HY=6,5, HZ=14,6 [cm]
 AX=8,77 [cm²]
 IX=0,28, IY=205,75, IZ=54,43 [cm⁴]
 Material=S235

IPE 120



HY=6,4, HZ=12,0 [cm]
 AX=13,21 [cm²]
 IX=1,69, IY=318,00, IZ=27,67 [cm⁴]
 Material=S235

K 40x40x2



HY=4,0, HZ=4,0 [cm]
 AX=3,04 [cm²]
 IX=10,97, IY=7,34, IZ=7,34 [cm⁴]
 Material=S235

K 80x40x3



HY=4,0, HZ=8,0 [cm]
 AX=6,84 [cm²]
 IX=42,72, IY=55,85, IZ=18,43 [cm⁴]
 Material=S235

K 70x50x4



HY=5,0, HZ=7,0 [cm]
 AX=8,96 [cm²]
 IX=65,84, IY=59,50, IZ=34,64 [cm⁴]
 Material=S235

6.5 Data – Bars

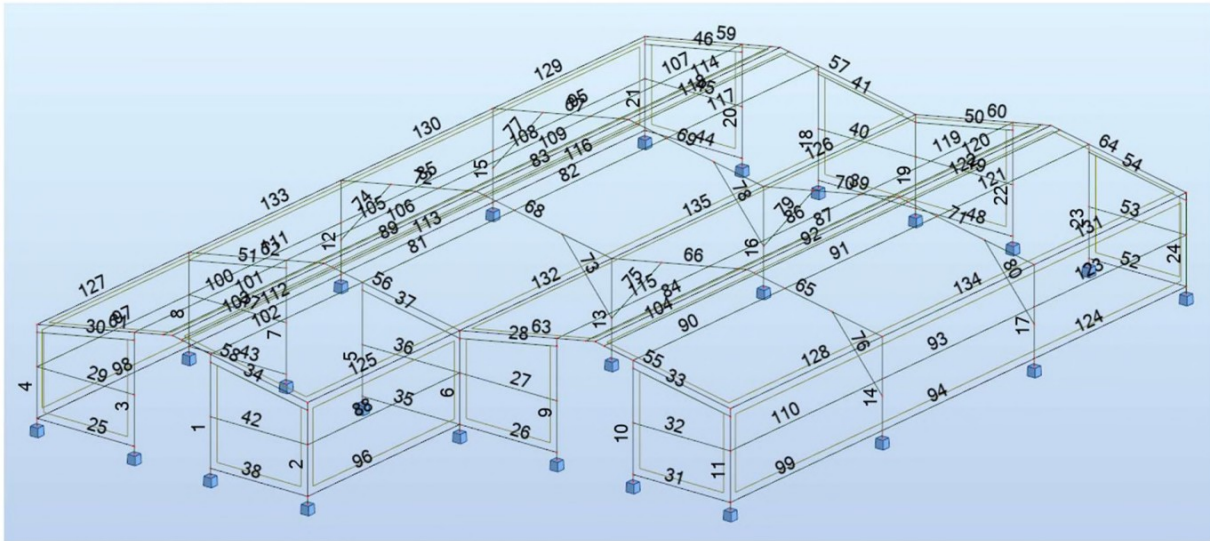


Figure of structure with bar numbers

| Member | Node 1 | Node 2 | Section | Material | Length (m) | Gamma (Deg) | Type |
|--------|--------|--------|-----------|----------|------------|-------------|--------|
| 1 | 1 | 2 | K 40x40x2 | S235 | 2,12 | 0,0 | Column |
| 2 | 3 | 4 | K 40x40x2 | S235 | 1,77 | 0,0 | Column |
| 3 | 12 | 13 | K 40x40x2 | S235 | 2,12 | 180,0 | Column |
| 4 | 14 | 15 | K 40x40x2 | S235 | 1,77 | 180,0 | Column |
| 5 | 22 | 23 | K 40x40x2 | S235 | 2,12 | 0,0 | Column |
| 6 | 24 | 25 | K 40x40x2 | S235 | 1,77 | 180,0 | Column |
| 7 | 33 | 34 | K 40x40x2 | S235 | 2,12 | -180,0 | Column |
| 8 | 35 | 36 | K 40x40x2 | S235 | 1,77 | -180,0 | Column |
| 9 | 43 | 44 | K 40x40x2 | S235 | 2,12 | 180,0 | Column |
| 10 | 49 | 50 | K 40x40x2 | S235 | 2,12 | 0,0 | Column |
| 11 | 51 | 52 | K 40x40x2 | S235 | 1,77 | 0,0 | Column |
| 12 | 69 | 66 | IPE 120 | S235 | 1,77 | 180,0 | Column |
| 13 | 77 | 74 | IPE 120 | S235 | 1,77 | 180,0 | Column |
| 14 | 84 | 83 | IPE 120 | S235 | 1,77 | 0,0 | Column |
| 15 | 99 | 96 | IPE 120 | S235 | 1,77 | 180,0 | Column |
| 16 | 106 | 103 | IPE 120 | S235 | 1,77 | 180,0 | Column |
| 17 | 112 | 111 | IPE 120 | S235 | 1,77 | 0,0 | Column |
| 18 | 120 | 121 | K 40x40x2 | S235 | 2,12 | 0,0 | Column |
| 19 | 122 | 123 | K 40x40x2 | S235 | 1,77 | 180,0 | Column |
| 20 | 131 | 132 | K 40x40x2 | S235 | 2,12 | 180,0 | Column |
| 21 | 133 | 134 | K 40x40x2 | S235 | 1,77 | 180,0 | Column |
| 22 | 140 | 141 | K 40x40x2 | S235 | 2,12 | 180,0 | Column |
| 23 | 146 | 147 | K 40x40x2 | S235 | 2,12 | 0,0 | Column |
| 24 | 148 | 149 | K 40x40x2 | S235 | 1,77 | 0,0 | Column |
| 25 | 16 | 17 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 26 | 45 | 27 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 27 | 46 | 29 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 28 | 47 | 31 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 29 | 18 | 19 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 30 | 20 | 21 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 31 | 53 | 54 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 32 | 55 | 56 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 33 | 57 | 58 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 34 | 9 | 10 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 35 | 26 | 27 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 36 | 28 | 29 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |

| Member | Node 1 | Node 2 | Section | Material | Length (m) | Gamma (Deg) | Type |
|--------|--------|--------|--------------|----------|------------|-------------|------|
| 37 | 30 | 31 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 38 | 5 | 6 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 39 | 124 | 125 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 40 | 126 | 127 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 41 | 128 | 129 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 42 | 7 | 8 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 43 | 37 | 38 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 44 | 135 | 136 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 45 | 137 | 119 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 46 | 138 | 139 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 47 | 39 | 40 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 48 | 142 | 125 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 49 | 143 | 127 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 50 | 144 | 129 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 51 | 41 | 42 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 52 | 150 | 151 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 53 | 152 | 153 | K 40x20x2 | S235 | 2,00 | 0,0 | Beam |
| 54 | 154 | 155 | K 40x20x2 | S235 | 2,03 | 0,0 | Beam |
| 55 | 48 | 52 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 56 | 32 | 25 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 57 | 130 | 123 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 58 | 11 | 4 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 59 | 130 | 134 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 60 | 145 | 123 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 61 | 11 | 15 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 62 | 32 | 36 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 63 | 48 | 25 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 64 | 145 | 149 | K 80x40x3 | S235 | 2,82 | 0,0 | Beam |
| 65 | 79 | 83 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 66 | 79 | 74 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 67 | 95 | 96 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 68 | 65 | 74 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 69 | 95 | 103 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 70 | 108 | 103 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 71 | 108 | 111 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 72 | 65 | 66 | K 70x50x4 | S235 | 2,82 | 0,0 | Beam |
| 73 | 72 | 73 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 74 | 63 | 64 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 75 | 78 | 73 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 76 | 85 | 86 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 77 | 93 | 94 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 78 | 101 | 102 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 79 | 107 | 102 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 80 | 113 | 114 | K 40x40x2 | S235 | 1,59 | 0,0 | Beam |
| 81 | 23 | 75 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 82 | 75 | 104 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 83 | 76 | 105 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 84 | 82 | 81 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 85 | 92 | 70 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 86 | 109 | 80 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 87 | 110 | 82 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 88 | 8 | 29 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 89 | 61 | 76 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 90 | 50 | 87 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 91 | 87 | 115 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 92 | 89 | 116 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |

| Member | Node 1 | Node 2 | Section | Material | Length (m) | Gamma (Deg) | Type |
|--------|--------|--------|---------------|----------|------------|-------------|------|
| 93 | 90 | 117 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 94 | 91 | 118 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 95 | 119 | 92 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 96 | 6 | 27 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 97 | 40 | 19 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 98 | 38 | 17 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 99 | 54 | 91 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 100 | 34 | 13 | TELG 80x40x3 | S235 | 4,00 | 190,0 | Beam |
| 101 | 59 | 60 | TELG 80x40x3 | S235 | 4,00 | 190,0 | Beam |
| 102 | 2 | 23 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 103 | 62 | 61 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 104 | 88 | 89 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 105 | 67 | 34 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 106 | 68 | 59 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 107 | 132 | 97 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 108 | 97 | 67 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 109 | 98 | 68 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 110 | 56 | 90 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 111 | 70 | 40 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 112 | 71 | 38 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 113 | 100 | 71 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 114 | 156 | 98 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 115 | 80 | 44 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 116 | 136 | 100 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 117 | 104 | 121 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 118 | 105 | 157 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 119 | 141 | 109 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 120 | 158 | 110 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 121 | 115 | 147 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 122 | 116 | 159 | TELG 80x40x3 | S235 | 4,00 | -170,0 | Beam |
| 123 | 117 | 153 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 124 | 118 | 151 | TELG 80x40x3 | S235 | 4,00 | 0,0 | Beam |
| 125 | 4 | 25 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 126 | 103 | 123 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 127 | 15 | 36 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 128 | 83 | 52 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 129 | 96 | 134 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 130 | 96 | 66 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 131 | 111 | 149 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 132 | 74 | 25 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 133 | 66 | 36 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 134 | 111 | 83 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |
| 135 | 103 | 74 | TELG 100x65x3 | S235 | 4,00 | 90,0 | Beam |

6.6 Data – Nodes

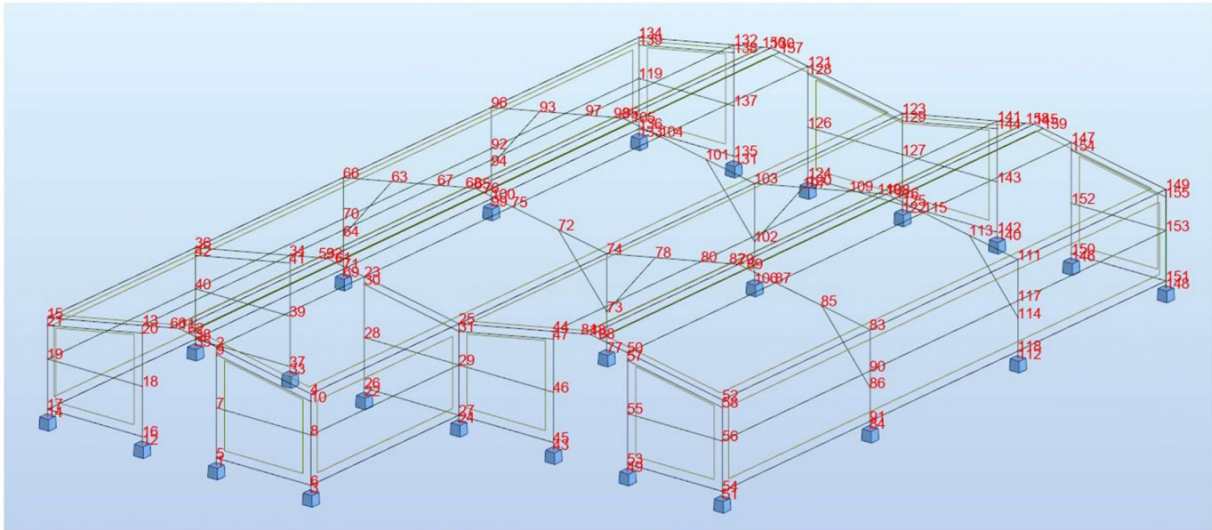


Figure of structure with node numbers

| Node | X (m) | Y (m) | Z (m) | Support code | Support |
|------|-------|-------|-------|--------------|---------|
| 1 | 3,56 | 0,0 | 0,0 | xxxxxx | Vast |
| 2 | 3,56 | 0,0 | 2,12 | | |
| 3 | 5,56 | 0,0 | 0,0 | xxxxxx | Vast |
| 4 | 5,56 | 0,0 | 1,77 | | |
| 5 | 3,56 | 0,0 | 0,13 | | |
| 6 | 5,56 | 0,0 | 0,13 | | |
| 7 | 3,56 | 0,0 | 1,03 | | |
| 8 | 5,56 | 0,0 | 1,03 | | |
| 9 | 3,56 | 0,0 | 1,98 | | |
| 10 | 5,56 | 0,0 | 1,63 | | |
| 11 | 2,78 | 0,0 | 2,26 | | |
| 12 | 2,00 | 0,0 | 0,0 | xxxxxx | Vast |
| 13 | 2,00 | 0,0 | 2,12 | | |
| 14 | -0,00 | 0,0 | 0,0 | xxxxxx | Vast |
| 15 | -0,00 | 0,0 | 1,77 | | |
| 16 | 2,00 | 0,0 | 0,13 | | |
| 17 | -0,00 | 0,0 | 0,13 | | |
| 18 | 2,00 | 0,0 | 1,03 | | |
| 19 | -0,00 | 0,0 | 1,03 | | |
| 20 | 2,00 | 0,0 | 1,98 | | |
| 21 | -0,00 | 0,0 | 1,63 | | |
| 22 | 3,56 | 4,00 | 0,0 | xxxxxx | Vast |
| 23 | 3,56 | 4,00 | 2,12 | | |
| 24 | 5,56 | 4,00 | 0,0 | xxxxxx | Vast |
| 25 | 5,56 | 4,00 | 1,77 | | |
| 26 | 3,56 | 4,00 | 0,13 | | |
| 27 | 5,56 | 4,00 | 0,13 | | |
| 28 | 3,56 | 4,00 | 1,03 | | |
| 29 | 5,56 | 4,00 | 1,03 | | |
| 30 | 3,56 | 4,00 | 1,98 | | |
| 31 | 5,56 | 4,00 | 1,63 | | |
| 32 | 2,78 | 4,00 | 2,26 | | |
| 33 | 2,00 | 4,00 | 0,0 | xxxxxx | Vast |
| 34 | 2,00 | 4,00 | 2,12 | | |
| 35 | -0,00 | 4,00 | 0,0 | xxxxxx | Vast |
| 36 | -0,00 | 4,00 | 1,77 | | |
| 37 | 2,00 | 4,00 | 0,13 | | |

| Node | X (m) | Y (m) | Z (m) | Support code | Support |
|------|-------|-------|-------|--------------|---------|
| 38 | -0,00 | 4,00 | 0,13 | | |
| 39 | 2,00 | 4,00 | 1,03 | | |
| 40 | -0,00 | 4,00 | 1,03 | | |
| 41 | 2,00 | 4,00 | 1,98 | | |
| 42 | -0,00 | 4,00 | 1,63 | | |
| 43 | 7,56 | 4,00 | 0,0 | xxxxxx | Vast |
| 44 | 7,56 | 4,00 | 2,12 | | |
| 45 | 7,56 | 4,00 | 0,13 | | |
| 46 | 7,56 | 4,00 | 1,03 | | |
| 47 | 7,56 | 4,00 | 1,98 | | |
| 48 | 8,34 | 4,00 | 2,26 | | |
| 49 | 9,12 | 4,00 | 0,0 | xxxxxx | Vast |
| 50 | 9,12 | 4,00 | 2,12 | | |
| 51 | 11,12 | 4,00 | 0,0 | xxxxxx | Vast |
| 52 | 11,12 | 4,00 | 1,77 | | |
| 53 | 9,12 | 4,00 | 0,13 | | |
| 54 | 11,12 | 4,00 | 0,13 | | |
| 55 | 9,12 | 4,00 | 1,03 | | |
| 56 | 11,12 | 4,00 | 1,03 | | |
| 57 | 9,12 | 4,00 | 1,98 | | |
| 58 | 11,12 | 4,00 | 1,63 | | |
| 59 | 2,60 | 4,00 | 2,23 | | |
| 60 | 2,60 | 0,0 | 2,23 | | |
| 61 | 2,96 | 4,00 | 2,23 | | |
| 62 | 2,96 | 0,0 | 2,23 | | |
| 63 | 1,03 | 8,00 | 1,95 | | |
| 64 | 0,0 | 8,00 | 0,73 | | |
| 65 | 2,78 | 8,00 | 2,26 | | |
| 66 | -0,00 | 8,00 | 1,77 | | |
| 67 | 2,00 | 8,00 | 2,12 | | |
| 68 | 2,60 | 8,00 | 2,23 | | |
| 69 | -0,00 | 8,00 | 0,0 | xxxxxx | Vast |
| 70 | -0,00 | 8,00 | 1,03 | | |
| 71 | -0,00 | 8,00 | 0,13 | | |
| 72 | 4,54 | 8,00 | 1,95 | | |
| 73 | 5,56 | 8,00 | 0,73 | | |
| 74 | 5,56 | 8,00 | 1,77 | | |
| 75 | 3,56 | 8,00 | 2,12 | | |
| 76 | 2,96 | 8,00 | 2,23 | | |
| 77 | 5,56 | 8,00 | 0,0 | xxxxxx | Vast |
| 78 | 6,59 | 8,00 | 1,95 | | |
| 79 | 8,34 | 8,00 | 2,26 | | |
| 80 | 7,56 | 8,00 | 2,12 | | |
| 81 | 8,16 | 4,00 | 2,23 | | |
| 82 | 8,16 | 8,00 | 2,23 | | |
| 83 | 11,12 | 8,00 | 1,77 | | |
| 84 | 11,12 | 8,00 | 0,0 | xxxxxx | Vast |
| 85 | 10,10 | 8,00 | 1,95 | | |
| 86 | 11,12 | 8,00 | 0,73 | | |
| 87 | 9,12 | 8,00 | 2,12 | | |
| 88 | 8,53 | 4,00 | 2,23 | | |
| 89 | 8,53 | 8,00 | 2,23 | | |
| 90 | 11,12 | 8,00 | 1,03 | | |
| 91 | 11,12 | 8,00 | 0,13 | | |
| 92 | -0,00 | 12,00 | 1,03 | | |
| 93 | 1,03 | 12,00 | 1,95 | | |
| 94 | 0,0 | 12,00 | 0,73 | | |

| Node | X (m) | Y (m) | Z (m) | Support code | Support |
|------|-------|-------|-------|--------------|---------|
| 95 | 2,78 | 12,00 | 2,26 | | |
| 96 | -0,00 | 12,00 | 1,77 | | |
| 97 | 2,00 | 12,00 | 2,12 | | |
| 98 | 2,60 | 12,00 | 2,23 | | |
| 99 | -0,00 | 12,00 | 0,0 | xxxxxx | Vast |
| 100 | -0,00 | 12,00 | 0,13 | | |
| 101 | 4,54 | 12,00 | 1,95 | | |
| 102 | 5,56 | 12,00 | 0,73 | | |
| 103 | 5,56 | 12,00 | 1,77 | | |
| 104 | 3,56 | 12,00 | 2,12 | | |
| 105 | 2,96 | 12,00 | 2,23 | | |
| 106 | 5,56 | 12,00 | 0,0 | xxxxxx | Vast |
| 107 | 6,59 | 12,00 | 1,95 | | |
| 108 | 8,34 | 12,00 | 2,26 | | |
| 109 | 7,56 | 12,00 | 2,12 | | |
| 110 | 8,16 | 12,00 | 2,23 | | |
| 111 | 11,12 | 12,00 | 1,77 | | |
| 112 | 11,12 | 12,00 | 0,0 | xxxxxx | Vast |
| 113 | 10,10 | 12,00 | 1,95 | | |
| 114 | 11,12 | 12,00 | 0,73 | | |
| 115 | 9,12 | 12,00 | 2,12 | | |
| 116 | 8,53 | 12,00 | 2,23 | | |
| 117 | 11,12 | 12,00 | 1,03 | | |
| 118 | 11,12 | 12,00 | 0,13 | | |
| 119 | -0,00 | 16,00 | 1,03 | | |
| 120 | 3,56 | 16,00 | 0,0 | xxxxxx | Vast |
| 121 | 3,56 | 16,00 | 2,12 | | |
| 122 | 5,56 | 16,00 | 0,0 | xxxxxx | Vast |
| 123 | 5,56 | 16,00 | 1,77 | | |
| 124 | 3,56 | 16,00 | 0,13 | | |
| 125 | 5,56 | 16,00 | 0,13 | | |
| 126 | 3,56 | 16,00 | 1,03 | | |
| 127 | 5,56 | 16,00 | 1,03 | | |
| 128 | 3,56 | 16,00 | 1,98 | | |
| 129 | 5,56 | 16,00 | 1,63 | | |
| 130 | 2,78 | 16,00 | 2,26 | | |
| 131 | 2,00 | 16,00 | 0,0 | xxxxxx | Vast |
| 132 | 2,00 | 16,00 | 2,12 | | |
| 133 | -0,00 | 16,00 | 0,0 | xxxxxx | Vast |
| 134 | -0,00 | 16,00 | 1,77 | | |
| 135 | 2,00 | 16,00 | 0,13 | | |
| 136 | -0,00 | 16,00 | 0,13 | | |
| 137 | 2,00 | 16,00 | 1,03 | | |
| 138 | 2,00 | 16,00 | 1,98 | | |
| 139 | -0,00 | 16,00 | 1,63 | | |
| 140 | 7,56 | 16,00 | 0,0 | xxxxxx | Vast |
| 141 | 7,56 | 16,00 | 2,12 | | |
| 142 | 7,56 | 16,00 | 0,13 | | |
| 143 | 7,56 | 16,00 | 1,03 | | |
| 144 | 7,56 | 16,00 | 1,98 | | |
| 145 | 8,34 | 16,00 | 2,26 | | |
| 146 | 9,12 | 16,00 | 0,0 | xxxxxx | Vast |
| 147 | 9,12 | 16,00 | 2,12 | | |
| 148 | 11,12 | 16,00 | 0,0 | xxxxxx | Vast |
| 149 | 11,12 | 16,00 | 1,77 | | |
| 150 | 9,12 | 16,00 | 0,13 | | |
| 151 | 11,12 | 16,00 | 0,13 | | |

| Node | X (m) | Y (m) | Z (m) | Support code | Support |
|------|-------|-------|-------|--------------|---------|
| 152 | 9,12 | 16,00 | 1,03 | | |
| 153 | 11,12 | 16,00 | 1,03 | | |
| 154 | 9,12 | 16,00 | 1,98 | | |
| 155 | 11,12 | 16,00 | 1,63 | | |
| 156 | 2,60 | 16,00 | 2,23 | | |
| 157 | 2,96 | 16,00 | 2,23 | | |
| 158 | 8,16 | 16,00 | 2,23 | | |
| 159 | 8,53 | 16,00 | 2,23 | | |

6.7 Data – Supports

| Support name | List of nodes | List of edges | List of objects | Support conditions |
|--------------|---|---------------|-----------------|--------------------|
| Vast | 1 3 12 14 22 24 33 35 43 49 51 69 77 84 99 106 112 120 122 131 133 140 146 148 | | | UX UY UZ RX RY RZ |

6.8 Loads – Cases

| Case | Label | Case name | Nature | Analysis type |
|------|-------|--|------------|-----------------|
| 1 | DL1 | DL1 | Structural | Static - Linear |
| 2 | SN1 | SN1 | snow | Static - Linear |
| 3 | WIND1 | Wind X+ 28,06 m/s (f =1.00) Simulation | wind | Static - Linear |
| 4 | WIND2 | Wind Y+ 28,06 m/s (f =1.00) Simulation | wind | Static - Linear |
| 5 | WIND3 | Wind X- 28,06 m/s (f =1.00) Simulation | wind | Static - Linear |
| 6 | WIND4 | Wind Y- 28,06 m/s (f =1.00) Simulation | wind | Static - Linear |
| 7 | | ULS | | Static - Linear |
| 8 | | ULS+ | | Static - Linear |
| 9 | | ULS- | | Static - Linear |
| 10 | | SLS | | Static - Linear |
| 11 | | SLS+ | | Static - Linear |
| 12 | | SLS- | | Static - Linear |
| 13 | | SLS:CHR | | Static - Linear |
| 14 | | SLS:CHR+ | | Static - Linear |
| 15 | | SLS:CHR- | | Static - Linear |
| 16 | | SLS:FRE | | Static - Linear |
| 17 | | SLS:FRE+ | | Static - Linear |
| 18 | | SLS:FRE- | | Static - Linear |
| 19 | | SLS:QPR | | Static - Linear |

6.9 Loads – Values

| Case | Load type | List | Load values |
|------|--------------|----------|-------------------------|
| 1 | self-weight | 1to149 | PZ Negative Factor=1,00 |
| 1 | (FE) uniform | 140to143 | PZ=-0,10(kN/m2) |
| 2 | (FE) uniform | 140to143 | PZ=-0,56(kN/m2) |
| 3 | (FE) uniform | 136 | PZ=-0,08(kN/m2) local |
| 3 | (FE) uniform | 137 | PZ=-0,20(kN/m2) local |
| 3 | (FE) uniform | 138 | PZ=0,08(kN/m2) local |
| 3 | (FE) uniform | 139 | PZ=0,03(kN/m2) local |
| 3 | (FE) uniform | 140 | PZ=-0,00(kN/m2) local |
| 3 | (FE) uniform | 141 | PZ=-0,02(kN/m2) local |
| 3 | (FE) uniform | 142 | PZ=0,02(kN/m2) local |
| 3 | (FE) uniform | 143 | PZ=0,24(kN/m2) local |
| 3 | (FE) uniform | 144 | PZ=0,33(kN/m2) local |
| 3 | (FE) uniform | 145 | PZ=-0,02(kN/m2) local |
| 3 | (FE) uniform | 146 | PZ=-0,07(kN/m2) local |
| 3 | (FE) uniform | 147 | PZ=0,19(kN/m2) local |
| 3 | (FE) uniform | 148 | PZ=0,01(kN/m2) local |
| 3 | (FE) uniform | 149 | PZ=0,03(kN/m2) local |

| Case | Load type | List | Load values |
|------|----------------------|-------------|------------------------------------|
| 4 | (FE) uniform | 136 | PZ=0,28(kN/m ²) local |
| 4 | (FE) uniform | 137 | PZ=0,25(kN/m ²) local |
| 4 | (FE) uniform | 138 | PZ=-0,01(kN/m ²) local |
| 4 | (FE) uniform | 139 149 | PZ=0,13(kN/m ²) local |
| 4 | (FE) linear on edges | 140_EDGE(3) | PY=0,00(kN/m) PZ=0,10(kN/m) local |
| 4 | (FE) uniform | 140 | PZ=0,16(kN/m ²) local |
| 4 | (FE) uniform | 141 | PZ=0,18(kN/m ²) local |
| 4 | (FE) uniform | 142 | PZ=0,16(kN/m ²) local |
| 4 | (FE) linear on edges | 143_EDGE(1) | PY=-0,00(kN/m) PZ=0,09(kN/m) local |
| 4 | (FE) uniform | 143 | PZ=0,13(kN/m ²) local |
| 4 | (FE) uniform | 144 | PZ=-0,10(kN/m ²) local |
| 4 | (FE) uniform | 145 | PZ=0,05(kN/m ²) local |
| 4 | (FE) uniform | 146 | PZ=0,23(kN/m ²) local |
| 4 | (FE) uniform | 147 | PZ=0,11(kN/m ²) local |
| 4 | (FE) uniform | 148 | PZ=0,12(kN/m ²) local |
| 5 | (FE) uniform | 136 | PZ=-0,18(kN/m ²) local |
| 5 | (FE) uniform | 137 | PZ=-0,10(kN/m ²) local |
| 5 | (FE) uniform | 138 | PZ=-0,19(kN/m ²) local |
| 5 | (FE) uniform | 139 | PZ=-0,30(kN/m ²) local |
| 5 | (FE) uniform | 140 | PZ=0,24(kN/m ²) local |
| 5 | (FE) uniform | 141 | PZ=0,05(kN/m ²) local |
| 5 | (FE) uniform | 142 | PZ=0,07(kN/m ²) local |
| 5 | (FE) uniform | 143 | PZ=0,05(kN/m ²) local |
| 5 | (FE) uniform | 144 | PZ=-0,08(kN/m ²) local |
| 5 | (FE) uniform | 145 | PZ=0,09(kN/m ²) local |
| 5 | (FE) uniform | 146 | PZ=-0,06(kN/m ²) local |
| 5 | (FE) uniform | 147 | PZ=0,06(kN/m ²) local |
| 5 | (FE) uniform | 148 | PZ=0,05(kN/m ²) local |
| 5 | (FE) uniform | 149 | PZ=0,19(kN/m ²) local |
| 6 | (FE) uniform | 136 | PZ=-0,09(kN/m ²) local |
| 6 | (FE) uniform | 137 | PZ=-0,10(kN/m ²) local |
| 6 | (FE) uniform | 138 | PZ=0,12(kN/m ²) local |
| 6 | (FE) uniform | 139 | PZ=0,13(kN/m ²) local |
| 6 | (FE) linear on edges | 140_EDGE(1) | PY=-0,00(kN/m) PZ=0,10(kN/m) local |
| 6 | (FE) uniform | 140 | PZ=0,17(kN/m ²) local |
| 6 | (FE) linear on edges | 141_EDGE(3) | PY=-0,00(kN/m) PZ=0,12(kN/m) local |
| 6 | (FE) uniform | 141 | PZ=0,21(kN/m ²) local |
| 6 | (FE) linear on edges | 142_EDGE(1) | PY=0,00(kN/m) PZ=0,13(kN/m) local |
| 6 | (FE) uniform | 142 | PZ=0,19(kN/m ²) local |
| 6 | (FE) linear on edges | 143_EDGE(3) | PY=-0,00(kN/m) PZ=0,10(kN/m) local |
| 6 | (FE) uniform | 143 | PZ=0,16(kN/m ²) local |
| 6 | (FE) uniform | 144 | PZ=-0,12(kN/m ²) local |
| 6 | (FE) uniform | 145 | PZ=-0,15(kN/m ²) local |
| 6 | (FE) uniform | 146 | PZ=-0,14(kN/m ²) local |
| 6 | (FE) uniform | 147 | PZ=-0,24(kN/m ²) local |
| 6 | (FE) uniform | 148 | PZ=-0,22(kN/m ²) local |
| 6 | (FE) uniform | 149 | PZ=-0,24(kN/m ²) local |

6.10 Combinations

| Combinations/Comp. | Definition |
|--------------------|-----------------|
| ULS/ 1 | 1*1.35 |
| ULS/ 2 | 1*1.00 |
| ULS/ 3 | 1*1.20 |
| ULS/ 4 | 1*1.00 |
| ULS/ 5 | 1*1.20 + 3*1.50 |
| ULS/ 6 | 1*1.20 + 4*1.50 |
| ULS/ 7 | 1*1.20 + 5*1.50 |
| ULS/ 8 | 1*1.20 + 6*1.50 |
| ULS/ 9 | 1*1.00 + 3*1.50 |
| ULS/ 10 | 1*1.00 + 4*1.50 |
| ULS/ 11 | 1*1.00 + 5*1.50 |
| ULS/ 12 | 1*1.00 + 6*1.50 |
| ULS/ 13 | 1*1.20 + 2*1.50 |
| ULS/ 14 | 1*1.00 + 2*1.50 |
| SLS:CHR/ 1 | 1*1.00 |
| SLS:CHR/ 2 | 1*1.00 + 3*1.00 |
| SLS:CHR/ 3 | 1*1.00 + 4*1.00 |
| SLS:CHR/ 4 | 1*1.00 + 5*1.00 |
| SLS:CHR/ 5 | 1*1.00 + 6*1.00 |
| SLS:CHR/ 6 | 1*1.00 + 2*1.00 |
| SLS:FRE/ 7 | 1*1.00 |
| SLS:FRE/ 8 | 1*1.00 + 3*0.20 |
| SLS:FRE/ 9 | 1*1.00 + 4*0.20 |
| SLS:FRE/ 10 | 1*1.00 + 5*0.20 |
| SLS:FRE/ 11 | 1*1.00 + 6*0.20 |
| SLS:FRE/ 12 | 1*1.00 + 2*0.20 |
| SLS:QPR/ 13 | 1*1.00 |
| SLS:CHR/ 1 | 1*1.00 |
| SLS:CHR/ 2 | 1*1.00 + 3*1.00 |
| SLS:CHR/ 3 | 1*1.00 + 4*1.00 |
| SLS:CHR/ 4 | 1*1.00 + 5*1.00 |
| SLS:CHR/ 5 | 1*1.00 + 6*1.00 |
| SLS:CHR/ 6 | 1*1.00 + 2*1.00 |
| SLS:FRE/ 1 | 1*1.00 |
| SLS:FRE/ 2 | 1*1.00 + 3*0.20 |
| SLS:FRE/ 3 | 1*1.00 + 4*0.20 |
| SLS:FRE/ 4 | 1*1.00 + 5*0.20 |
| SLS:FRE/ 5 | 1*1.00 + 6*0.20 |
| SLS:FRE/ 6 | 1*1.00 + 2*0.20 |
| SLS:QPR/ 1 | 1*1.00 |

6.11 Reactions – Values

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|--------------|---------|---------|---------|----------|----------|----------|
| 1/ 1 | 0,03 | 0,03 | 0,61 | -0,02 | -0,00 | -0,00 |
| 1/ 2 | -0,01 | 0,13 | 1,74 | -0,09 | -0,01 | -0,00 |
| 1/ 3 | -0,14 | 0,06 | -0,21 | -0,02 | -0,08 | 0,01 |
| 1/ 4 | 0,04 | -0,34 | -0,45 | 0,17 | 0,03 | -0,06 |
| 1/ 5 | 0,22 | 0,17 | -0,17 | -0,06 | 0,10 | 0,05 |
| 1/ 6 | -0,10 | 0,07 | -0,50 | -0,04 | -0,02 | 0,02 |
| 1/ ULS+ | 0,36 | 0,29 | 3,35 | 0,23 | 0,15 | 0,07 |
| 1/ ULS- | -0,18 | -0,48 | -0,14 | -0,16 | -0,12 | -0,09 |
| 1/ SLS+ | 0,25 | 0,20 | 2,35 | 0,14 | 0,10 | 0,05 |
| 1/ SLS- | -0,11 | -0,31 | 0,11 | -0,11 | -0,08 | -0,06 |
| 1/ SLS:CHR+ | 0,25 | 0,20 | 2,35 | 0,14 | 0,10 | 0,05 |
| 1/ SLS:CHR- | -0,11 | -0,31 | 0,11 | -0,11 | -0,08 | -0,06 |
| 1/ SLS:FRE+ | 0,07 | 0,07 | 0,96 | 0,01 | 0,02 | 0,01 |
| 1/ SLS:FRE- | -0,00 | -0,04 | 0,51 | -0,04 | -0,02 | -0,01 |
| 3/ 1 | -0,03 | 0,26 | 0,54 | -0,01 | -0,00 | -0,00 |
| 3/ 2 | -0,01 | 0,14 | 0,86 | -0,03 | -0,01 | -0,00 |
| 3/ 3 | -0,20 | 0,06 | 0,09 | -0,02 | -0,08 | 0,04 |
| 3/ 4 | 0,06 | -0,34 | -0,40 | 0,09 | 0,03 | 0,04 |
| 3/ 5 | 0,29 | 0,00 | -0,20 | 0,00 | 0,11 | -0,15 |
| 3/ 6 | -0,10 | 0,25 | -0,22 | -0,07 | -0,03 | 0,07 |
| 3/ ULS+ | 0,39 | 0,69 | 1,94 | 0,12 | 0,16 | 0,10 |
| 3/ ULS- | -0,35 | -0,24 | -0,05 | -0,12 | -0,13 | -0,23 |
| 3/ SLS+ | 0,25 | 0,51 | 1,40 | 0,08 | 0,10 | 0,06 |
| 3/ SLS- | -0,24 | -0,07 | 0,14 | -0,08 | -0,09 | -0,15 |
| 3/ SLS:CHR+ | 0,25 | 0,51 | 1,40 | 0,08 | 0,10 | 0,06 |
| 3/ SLS:CHR- | -0,24 | -0,07 | 0,14 | -0,08 | -0,09 | -0,15 |
| 3/ SLS:FRE+ | 0,02 | 0,31 | 0,71 | 0,01 | 0,02 | 0,01 |
| 3/ SLS:FRE- | -0,08 | 0,20 | 0,46 | -0,03 | -0,02 | -0,03 |
| 12/ 1 | -0,03 | 0,03 | 0,62 | -0,02 | 0,00 | 0,00 |
| 12/ 2 | 0,00 | 0,13 | 1,76 | -0,09 | 0,00 | 0,01 |
| 12/ 3 | -0,32 | 0,17 | -0,69 | -0,05 | -0,12 | -0,06 |
| 12/ 4 | 0,09 | -0,31 | -0,58 | 0,15 | 0,04 | 0,06 |
| 12/ 5 | 0,13 | 0,08 | -0,25 | -0,03 | 0,08 | -0,02 |
| 12/ 6 | 0,09 | 0,08 | -0,42 | -0,04 | 0,02 | -0,02 |
| 12/ ULS+ | 0,17 | 0,29 | 3,38 | 0,20 | 0,12 | 0,09 |
| 12/ ULS- | -0,51 | -0,44 | -0,42 | -0,17 | -0,18 | -0,09 |
| 12/ SLS+ | 0,11 | 0,20 | 2,38 | 0,13 | 0,08 | 0,06 |
| 12/ SLS- | -0,34 | -0,28 | -0,07 | -0,11 | -0,12 | -0,06 |
| 12/ SLS:CHR+ | 0,11 | 0,20 | 2,38 | 0,13 | 0,08 | 0,06 |
| 12/ SLS:CHR- | -0,34 | -0,28 | -0,07 | -0,11 | -0,12 | -0,06 |
| 12/ SLS:FRE+ | -0,00 | 0,06 | 0,97 | 0,01 | 0,02 | 0,01 |
| 12/ SLS:FRE- | -0,09 | -0,03 | 0,48 | -0,04 | -0,02 | -0,01 |
| 14/ 1 | 0,03 | 0,15 | 0,55 | 0,00 | 0,00 | 0,00 |
| 14/ 2 | 0,00 | 0,03 | 0,95 | 0,00 | 0,00 | 0,00 |
| 14/ 3 | -0,38 | 0,03 | -0,45 | -0,01 | -0,13 | 0,22 |
| 14/ 4 | 0,12 | -0,12 | -0,33 | 0,03 | 0,04 | -0,10 |
| 14/ 5 | 0,20 | 0,03 | 0,03 | -0,01 | 0,08 | -0,03 |
| 14/ 6 | 0,09 | 0,07 | -0,29 | -0,03 | 0,02 | -0,06 |
| 14/ ULS+ | 0,34 | 0,28 | 2,08 | 0,05 | 0,12 | 0,33 |
| 14/ ULS- | -0,54 | -0,04 | -0,13 | -0,04 | -0,20 | -0,15 |
| 14/ SLS+ | 0,23 | 0,22 | 1,49 | 0,04 | 0,08 | 0,22 |
| 14/ SLS- | -0,35 | 0,02 | 0,09 | -0,02 | -0,13 | -0,10 |
| 14/ SLS:CHR+ | 0,23 | 0,22 | 1,49 | 0,04 | 0,08 | 0,22 |
| 14/ SLS:CHR- | -0,35 | 0,02 | 0,09 | -0,02 | -0,13 | -0,10 |
| 14/ SLS:FRE+ | 0,07 | 0,16 | 0,74 | 0,01 | 0,02 | 0,04 |
| 14/ SLS:FRE- | -0,05 | 0,12 | 0,46 | -0,00 | -0,03 | -0,02 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|--------------|---------|---------|---------|----------|----------|----------|
| 22/ 1 | 0,02 | -0,00 | 1,33 | 0,00 | -0,00 | 0,00 |
| 22/ 2 | -0,01 | -0,00 | 4,66 | 0,00 | -0,00 | 0,00 |
| 22/ 3 | -0,10 | 0,01 | -0,58 | -0,01 | -0,07 | 0,00 |
| 22/ 4 | 0,02 | -0,04 | -1,20 | 0,05 | 0,01 | 0,00 |
| 22/ 5 | 0,16 | -0,01 | -0,51 | 0,00 | 0,08 | -0,01 |
| 22/ 6 | -0,07 | 0,06 | -1,41 | -0,05 | -0,02 | 0,01 |
| 22/ ULS+ | 0,26 | 0,09 | 8,59 | 0,07 | 0,12 | 0,01 |
| 22/ ULS- | -0,13 | -0,07 | -0,79 | -0,08 | -0,10 | -0,02 |
| 22/ SLS+ | 0,18 | 0,06 | 5,99 | 0,05 | 0,08 | 0,01 |
| 22/ SLS- | -0,08 | -0,04 | -0,09 | -0,05 | -0,07 | -0,01 |
| 22/ SLS:CHR+ | 0,18 | 0,06 | 5,99 | 0,05 | 0,08 | 0,01 |
| 22/ SLS:CHR- | -0,08 | -0,04 | -0,09 | -0,05 | -0,07 | -0,01 |
| 22/ SLS:FRE+ | 0,05 | 0,01 | 2,26 | 0,01 | 0,01 | 0,00 |
| 22/ SLS:FRE- | 0,00 | -0,01 | 1,04 | -0,01 | -0,01 | -0,00 |
| 24/ 1 | -0,00 | -0,21 | 1,24 | -0,01 | -0,00 | 0,00 |
| 24/ 2 | -0,00 | 0,09 | 3,44 | -0,03 | -0,00 | 0,00 |
| 24/ 3 | -0,23 | 0,07 | 0,08 | -0,01 | -0,07 | -0,04 |
| 24/ 4 | 0,04 | -0,32 | -1,08 | 0,09 | 0,01 | -0,01 |
| 24/ 5 | 0,29 | -0,00 | -0,39 | 0,00 | 0,09 | 0,11 |
| 24/ 6 | -0,09 | 0,27 | -1,45 | -0,07 | -0,02 | -0,05 |
| 24/ ULS+ | 0,44 | 0,20 | 6,65 | 0,12 | 0,13 | 0,16 |
| 24/ ULS- | -0,35 | -0,73 | -0,93 | -0,11 | -0,11 | -0,08 |
| 24/ SLS+ | 0,29 | 0,06 | 4,68 | 0,08 | 0,09 | 0,11 |
| 24/ SLS- | -0,23 | -0,53 | -0,21 | -0,08 | -0,07 | -0,05 |
| 24/ SLS:CHR+ | 0,29 | 0,06 | 4,68 | 0,08 | 0,09 | 0,11 |
| 24/ SLS:CHR- | -0,23 | -0,53 | -0,21 | -0,08 | -0,07 | -0,05 |
| 24/ SLS:FRE+ | 0,06 | -0,15 | 1,93 | 0,01 | 0,02 | 0,02 |
| 24/ SLS:FRE- | -0,05 | -0,27 | 0,95 | -0,02 | -0,01 | -0,01 |
| 33/ 1 | -0,02 | -0,00 | 1,34 | 0,00 | 0,00 | -0,00 |
| 33/ 2 | 0,03 | -0,01 | 4,71 | 0,01 | 0,01 | -0,00 |
| 33/ 3 | -0,61 | 0,00 | -1,92 | -0,00 | -0,19 | 0,00 |
| 33/ 4 | 0,17 | -0,03 | -1,04 | 0,04 | 0,05 | -0,00 |
| 33/ 5 | 0,19 | 0,01 | -0,47 | -0,01 | 0,09 | -0,00 |
| 33/ 6 | 0,19 | 0,04 | -1,22 | -0,04 | 0,04 | 0,00 |
| 33/ ULS+ | 0,27 | 0,06 | 8,67 | 0,06 | 0,13 | 0,00 |
| 33/ ULS- | -0,95 | -0,05 | -1,55 | -0,06 | -0,28 | -0,00 |
| 33/ SLS+ | 0,17 | 0,04 | 6,05 | 0,04 | 0,09 | 0,00 |
| 33/ SLS- | -0,64 | -0,03 | -0,59 | -0,04 | -0,19 | -0,00 |
| 33/ SLS:CHR+ | 0,17 | 0,04 | 6,05 | 0,04 | 0,09 | 0,00 |
| 33/ SLS:CHR- | -0,64 | -0,03 | -0,59 | -0,04 | -0,19 | -0,00 |
| 33/ SLS:FRE+ | 0,02 | 0,01 | 2,28 | 0,01 | 0,02 | 0,00 |
| 33/ SLS:FRE- | -0,14 | -0,01 | 0,95 | -0,01 | -0,03 | -0,00 |
| 35/ 1 | 0,04 | -0,10 | 1,08 | 0,01 | 0,01 | -0,00 |
| 35/ 2 | 0,03 | -0,06 | 2,24 | 0,00 | 0,01 | -0,00 |
| 35/ 3 | -0,67 | 0,07 | -0,86 | -0,01 | -0,22 | -0,02 |
| 35/ 4 | 0,18 | -0,21 | -0,62 | 0,03 | 0,06 | 0,01 |
| 35/ 5 | 0,25 | 0,04 | -0,13 | -0,00 | 0,09 | 0,00 |
| 35/ 6 | 0,18 | 0,20 | -0,77 | -0,03 | 0,05 | 0,01 |
| 35/ ULS+ | 0,42 | 0,21 | 4,65 | 0,05 | 0,14 | 0,02 |
| 35/ ULS- | -0,97 | -0,44 | -0,21 | -0,04 | -0,32 | -0,04 |
| 35/ SLS+ | 0,29 | 0,11 | 3,32 | 0,04 | 0,10 | 0,01 |
| 35/ SLS- | -0,63 | -0,31 | 0,22 | -0,02 | -0,21 | -0,02 |
| 35/ SLS:CHR+ | 0,29 | 0,11 | 3,32 | 0,04 | 0,10 | 0,01 |
| 35/ SLS:CHR- | -0,63 | -0,31 | 0,22 | -0,02 | -0,21 | -0,02 |
| 35/ SLS:FRE+ | 0,09 | -0,06 | 1,53 | 0,01 | 0,02 | 0,00 |
| 35/ SLS:FRE- | -0,10 | -0,14 | 0,91 | 0,00 | -0,04 | -0,01 |
| 43/ 1 | -0,02 | 0,04 | 0,63 | -0,03 | -0,00 | 0,00 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|--------------|---------|---------|---------|----------|----------|----------|
| 43/ 2 | -0,00 | 0,17 | 1,81 | -0,12 | -0,00 | 0,01 |
| 43/ 3 | -0,10 | 0,02 | 0,07 | -0,01 | -0,07 | -0,00 |
| 43/ 4 | 0,02 | -0,14 | -0,52 | 0,10 | 0,01 | 0,01 |
| 43/ 5 | 0,16 | -0,10 | -0,27 | 0,05 | 0,08 | 0,01 |
| 43/ 6 | -0,07 | 0,12 | -0,56 | -0,06 | -0,02 | -0,03 |
| 43/ ULS+ | 0,21 | 0,30 | 3,47 | 0,12 | 0,12 | 0,02 |
| 43/ ULS- | -0,18 | -0,17 | -0,21 | -0,21 | -0,10 | -0,04 |
| 43/ SLS+ | 0,13 | 0,20 | 2,44 | 0,07 | 0,08 | 0,01 |
| 43/ SLS- | -0,12 | -0,10 | 0,07 | -0,14 | -0,07 | -0,03 |
| 43/ SLS:CHR+ | 0,13 | 0,20 | 2,44 | 0,07 | 0,08 | 0,01 |
| 43/ SLS:CHR- | -0,12 | -0,10 | 0,07 | -0,14 | -0,07 | -0,03 |
| 43/ SLS:FRE+ | 0,01 | 0,07 | 0,99 | -0,01 | 0,02 | 0,00 |
| 43/ SLS:FRE- | -0,04 | 0,01 | 0,52 | -0,05 | -0,01 | -0,00 |
| 49/ 1 | 0,03 | 0,04 | 0,64 | -0,03 | -0,00 | -0,00 |
| 49/ 2 | -0,01 | 0,16 | 1,86 | -0,11 | -0,00 | -0,01 |
| 49/ 3 | -0,09 | 0,07 | -0,09 | -0,03 | -0,07 | 0,01 |
| 49/ 4 | -0,08 | -0,30 | -0,63 | 0,15 | -0,01 | -0,05 |
| 49/ 5 | 0,29 | 0,01 | -0,73 | 0,03 | 0,11 | 0,03 |
| 49/ 6 | -0,10 | 0,11 | -0,51 | -0,06 | -0,03 | 0,02 |
| 49/ ULS+ | 0,46 | 0,29 | 3,56 | 0,20 | 0,16 | 0,05 |
| 49/ ULS- | -0,13 | -0,42 | -0,45 | -0,20 | -0,10 | -0,08 |
| 49/ SLS+ | 0,31 | 0,20 | 2,50 | 0,12 | 0,11 | 0,03 |
| 49/ SLS- | -0,08 | -0,26 | -0,08 | -0,14 | -0,07 | -0,05 |
| 49/ SLS:CHR+ | 0,31 | 0,20 | 2,50 | 0,12 | 0,11 | 0,03 |
| 49/ SLS:CHR- | -0,08 | -0,26 | -0,08 | -0,14 | -0,07 | -0,05 |
| 49/ SLS:FRE+ | 0,08 | 0,07 | 1,02 | 0,00 | 0,02 | 0,00 |
| 49/ SLS:FRE- | 0,01 | -0,02 | 0,50 | -0,05 | -0,01 | -0,01 |
| 51/ 1 | -0,03 | 0,16 | 0,54 | 0,00 | -0,00 | 0,00 |
| 51/ 2 | -0,01 | 0,05 | 0,93 | 0,00 | -0,00 | 0,00 |
| 51/ 3 | -0,15 | 0,02 | 0,13 | -0,00 | -0,07 | 0,00 |
| 51/ 4 | -0,07 | -0,17 | -0,48 | 0,03 | -0,01 | 0,11 |
| 51/ 5 | 0,34 | -0,05 | -0,46 | 0,01 | 0,12 | -0,18 |
| 51/ 6 | -0,11 | 0,15 | -0,27 | -0,04 | -0,03 | 0,05 |
| 51/ ULS+ | 0,48 | 0,42 | 2,04 | 0,06 | 0,17 | 0,17 |
| 51/ ULS- | -0,26 | -0,09 | -0,18 | -0,06 | -0,10 | -0,27 |
| 51/ SLS+ | 0,31 | 0,31 | 1,47 | 0,04 | 0,12 | 0,11 |
| 51/ SLS- | -0,18 | -0,01 | 0,06 | -0,04 | -0,07 | -0,18 |
| 51/ SLS:CHR+ | 0,31 | 0,31 | 1,47 | 0,04 | 0,12 | 0,11 |
| 51/ SLS:CHR- | -0,18 | -0,01 | 0,06 | -0,04 | -0,07 | -0,18 |
| 51/ SLS:FRE+ | 0,03 | 0,19 | 0,73 | 0,01 | 0,02 | 0,02 |
| 51/ SLS:FRE- | -0,06 | 0,13 | 0,45 | -0,00 | -0,02 | -0,04 |
| 69/ 1 | 1,35 | -0,01 | 2,27 | -0,00 | 0,93 | -0,00 |
| 69/ 2 | 4,92 | -0,00 | 6,17 | -0,01 | 3,34 | -0,00 |
| 69/ 3 | -2,77 | 0,02 | -2,23 | -0,01 | -1,29 | -0,00 |
| 69/ 4 | -0,80 | -0,22 | -1,50 | 0,11 | -0,70 | -0,00 |
| 69/ 5 | -0,18 | 0,02 | -0,60 | -0,01 | -0,28 | 0,00 |
| 69/ 6 | -0,92 | 0,20 | -1,77 | -0,09 | -0,79 | 0,00 |
| 69/ ULS+ | 9,01 | 0,28 | 11,99 | 0,16 | 6,13 | 0,00 |
| 69/ ULS- | -2,80 | -0,34 | -1,08 | -0,14 | -1,00 | -0,00 |
| 69/ SLS+ | 6,28 | 0,18 | 8,44 | 0,11 | 4,27 | 0,00 |
| 69/ SLS- | -1,41 | -0,23 | 0,04 | -0,09 | -0,36 | -0,00 |
| 69/ SLS:CHR+ | 6,28 | 0,18 | 8,44 | 0,11 | 4,27 | 0,00 |
| 69/ SLS:CHR- | -1,41 | -0,23 | 0,04 | -0,09 | -0,36 | -0,00 |
| 69/ SLS:FRE+ | 2,34 | 0,03 | 3,51 | 0,02 | 1,59 | 0,00 |
| 69/ SLS:FRE- | 0,80 | -0,05 | 1,83 | -0,02 | 0,67 | -0,00 |
| 77/ 1 | 0,13 | -0,01 | 3,55 | 0,01 | 0,07 | -0,00 |
| 77/ 2 | 0,50 | -0,06 | 12,46 | 0,04 | 0,27 | -0,00 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|---------------|---------|---------|---------|----------|----------|----------|
| 77/ 3 | 0,75 | 0,02 | -0,42 | -0,02 | 0,42 | -0,00 |
| 77/ 4 | -0,34 | -0,19 | -3,66 | 0,18 | -0,21 | 0,00 |
| 77/ 5 | -0,44 | -0,01 | -1,69 | 0,01 | -0,27 | -0,00 |
| 77/ 6 | -0,29 | 0,28 | -4,22 | -0,25 | -0,16 | 0,00 |
| 77/ ULS+ | 1,28 | 0,41 | 22,95 | 0,28 | 0,71 | 0,00 |
| 77/ ULS- | -0,53 | -0,30 | -2,78 | -0,37 | -0,34 | -0,00 |
| 77/ SLS+ | 0,88 | 0,27 | 16,01 | 0,19 | 0,49 | 0,00 |
| 77/ SLS- | -0,31 | -0,20 | -0,67 | -0,24 | -0,20 | -0,00 |
| 77/ SLS:CHR+ | 0,88 | 0,27 | 16,01 | 0,19 | 0,49 | 0,00 |
| 77/ SLS:CHR- | -0,31 | -0,20 | -0,67 | -0,24 | -0,20 | -0,00 |
| 77/ SLS:FRE+ | 0,28 | 0,04 | 6,04 | 0,04 | 0,15 | -0,00 |
| 77/ SLS:FRE- | 0,04 | -0,05 | 2,71 | -0,04 | 0,01 | -0,00 |
| 84/ 1 | -1,48 | -0,12 | 2,45 | 0,01 | -1,00 | 0,00 |
| 84/ 2 | -5,42 | -0,10 | 6,79 | -0,00 | -3,63 | 0,00 |
| 84/ 3 | -0,14 | 0,03 | 0,03 | -0,01 | -0,01 | -0,00 |
| 84/ 4 | 0,90 | -0,26 | -1,93 | 0,12 | 0,71 | -0,00 |
| 84/ 5 | 2,96 | -0,03 | -2,50 | 0,04 | 1,46 | 0,01 |
| 84/ 6 | 1,12 | 0,35 | -2,13 | -0,13 | 0,89 | -0,00 |
| 84/ ULS+ | 2,96 | 0,40 | 13,13 | 0,18 | 1,19 | 0,01 |
| 84/ ULS- | -9,92 | -0,54 | -1,31 | -0,19 | -6,64 | -0,01 |
| 84/ SLS+ | 1,48 | 0,23 | 9,24 | 0,12 | 0,46 | 0,01 |
| 84/ SLS- | -6,91 | -0,38 | -0,06 | -0,12 | -4,62 | -0,00 |
| 84/ SLS:CHR+ | 1,48 | 0,23 | 9,24 | 0,12 | 0,46 | 0,01 |
| 84/ SLS:CHR- | -6,91 | -0,38 | -0,06 | -0,12 | -4,62 | -0,00 |
| 84/ SLS:FRE+ | -0,89 | -0,05 | 3,81 | 0,03 | -0,70 | 0,00 |
| 84/ SLS:FRE- | -2,57 | -0,17 | 1,95 | -0,02 | -1,72 | -0,00 |
| 99/ 1 | 1,52 | 0,13 | 2,48 | -0,01 | 1,04 | 0,00 |
| 99/ 2 | 5,59 | 0,10 | 6,93 | -0,00 | 3,78 | 0,00 |
| 99/ 3 | -2,97 | -0,05 | -2,45 | -0,01 | -1,36 | 0,01 |
| 99/ 4 | -0,97 | -0,28 | -1,68 | 0,11 | -0,82 | -0,00 |
| 99/ 5 | -0,27 | -0,00 | -0,67 | -0,01 | -0,37 | -0,00 |
| 99/ 6 | -1,08 | 0,23 | -2,03 | -0,10 | -0,89 | -0,00 |
| 99/ ULS+ | 10,22 | 0,50 | 13,37 | 0,16 | 6,91 | 0,01 |
| 99/ ULS- | -2,93 | -0,29 | -1,19 | -0,16 | -1,00 | -0,00 |
| 99/ SLS+ | 7,11 | 0,36 | 9,41 | 0,10 | 4,82 | 0,01 |
| 99/ SLS- | -1,45 | -0,15 | 0,03 | -0,11 | -0,32 | -0,00 |
| 99/ SLS:CHR+ | 7,11 | 0,36 | 9,41 | 0,10 | 4,82 | 0,01 |
| 99/ SLS:CHR- | -1,45 | -0,15 | 0,03 | -0,11 | -0,32 | -0,00 |
| 99/ SLS:FRE+ | 2,64 | 0,17 | 3,87 | 0,01 | 1,79 | 0,00 |
| 99/ SLS:FRE- | 0,93 | 0,07 | 1,99 | -0,03 | 0,76 | -0,00 |
| 106/ 1 | -0,02 | 0,04 | 3,79 | -0,02 | -0,01 | 0,00 |
| 106/ 2 | -0,09 | 0,16 | 13,38 | -0,08 | -0,05 | 0,00 |
| 106/ 3 | 0,94 | 0,03 | -0,52 | -0,03 | 0,56 | 0,00 |
| 106/ 4 | -0,18 | -0,26 | -3,89 | 0,22 | -0,13 | 0,00 |
| 106/ 5 | -0,43 | -0,03 | -1,78 | 0,02 | -0,30 | -0,00 |
| 106/ 6 | -0,09 | 0,19 | -4,61 | -0,20 | -0,05 | 0,00 |
| 106/ ULS+ | 1,38 | 0,33 | 24,62 | 0,31 | 0,83 | 0,00 |
| 106/ ULS- | -0,68 | -0,35 | -3,12 | -0,32 | -0,47 | -0,00 |
| 106/ SLS+ | 0,91 | 0,22 | 17,17 | 0,20 | 0,55 | 0,00 |
| 106/ SLS- | -0,46 | -0,22 | -0,82 | -0,22 | -0,31 | -0,00 |
| 106/ SLS:CHR+ | 0,91 | 0,22 | 17,17 | 0,20 | 0,55 | 0,00 |
| 106/ SLS:CHR- | -0,46 | -0,22 | -0,82 | -0,22 | -0,31 | -0,00 |
| 106/ SLS:FRE+ | 0,16 | 0,07 | 6,46 | 0,03 | 0,10 | 0,00 |
| 106/ SLS:FRE- | -0,11 | -0,02 | 2,87 | -0,06 | -0,07 | -0,00 |
| 112/ 1 | -1,50 | 0,12 | 2,45 | -0,01 | -1,02 | -0,00 |
| 112/ 2 | -5,50 | 0,11 | 6,83 | 0,00 | -3,73 | -0,00 |
| 112/ 3 | -0,08 | 0,02 | 0,02 | -0,01 | 0,08 | 0,00 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|---------------|---------|---------|---------|----------|----------|----------|
| 112/ 4 | 0,94 | -0,31 | -1,92 | 0,11 | 0,75 | 0,00 |
| 112/ 5 | 2,93 | -0,16 | -2,49 | 0,04 | 1,42 | -0,01 |
| 112/ 6 | 1,12 | 0,30 | -2,16 | -0,13 | 0,91 | 0,00 |
| 112/ ULS+ | 2,89 | 0,60 | 13,19 | 0,16 | 1,10 | 0,01 |
| 112/ ULS- | -10,06 | -0,34 | -1,28 | -0,21 | -6,83 | -0,01 |
| 112/ SLS+ | 1,43 | 0,42 | 9,28 | 0,11 | 0,39 | 0,00 |
| 112/ SLS- | -7,01 | -0,18 | -0,03 | -0,14 | -4,76 | -0,01 |
| 112/ SLS:CHR+ | 1,43 | 0,42 | 9,28 | 0,11 | 0,39 | 0,00 |
| 112/ SLS:CHR- | -7,01 | -0,18 | -0,03 | -0,14 | -4,76 | -0,01 |
| 112/ SLS:FRE+ | -0,92 | 0,18 | 3,82 | 0,02 | -0,74 | 0,00 |
| 112/ SLS:FRE- | -2,60 | 0,06 | 1,96 | -0,03 | -1,77 | -0,00 |
| 120/ 1 | 0,02 | -0,04 | 0,63 | 0,03 | -0,00 | 0,00 |
| 120/ 2 | -0,00 | -0,18 | 1,80 | 0,12 | 0,00 | 0,00 |
| 120/ 3 | -0,02 | 0,01 | -0,21 | -0,01 | -0,02 | -0,00 |
| 120/ 4 | -0,00 | -0,10 | -0,44 | 0,05 | -0,00 | -0,03 |
| 120/ 5 | 0,02 | -0,01 | -0,20 | -0,01 | 0,02 | -0,01 |
| 120/ 6 | -0,00 | 0,31 | -0,76 | -0,16 | -0,00 | 0,05 |
| 120/ ULS+ | 0,06 | 0,42 | 3,45 | 0,22 | 0,03 | 0,07 |
| 120/ ULS- | -0,01 | -0,32 | -0,51 | -0,21 | -0,03 | -0,04 |
| 120/ SLS+ | 0,05 | 0,26 | 2,42 | 0,15 | 0,02 | 0,05 |
| 120/ SLS- | 0,00 | -0,22 | -0,13 | -0,13 | -0,02 | -0,02 |
| 120/ SLS:CHR+ | 0,05 | 0,26 | 2,42 | 0,15 | 0,02 | 0,05 |
| 120/ SLS:CHR- | 0,00 | -0,22 | -0,13 | -0,13 | -0,02 | -0,02 |
| 120/ SLS:FRE+ | 0,03 | 0,02 | 0,99 | 0,05 | 0,00 | 0,01 |
| 120/ SLS:FRE- | 0,02 | -0,08 | 0,47 | -0,00 | -0,00 | -0,00 |
| 122/ 1 | -0,00 | -0,06 | 0,68 | 0,04 | -0,00 | -0,00 |
| 122/ 2 | 0,00 | -0,27 | 1,88 | 0,16 | 0,00 | -0,00 |
| 122/ 3 | -0,07 | -0,01 | 0,04 | -0,00 | -0,02 | 0,00 |
| 122/ 4 | -0,01 | -0,17 | -0,64 | 0,06 | -0,00 | 0,00 |
| 122/ 5 | 0,07 | -0,05 | -0,18 | 0,01 | 0,02 | -0,00 |
| 122/ 6 | -0,00 | 0,54 | -1,01 | -0,23 | -0,00 | 0,00 |
| 122/ ULS+ | 0,11 | 0,74 | 3,63 | 0,29 | 0,04 | 0,00 |
| 122/ ULS- | -0,10 | -0,48 | -0,83 | -0,31 | -0,03 | -0,00 |
| 122/ SLS+ | 0,07 | 0,47 | 2,55 | 0,20 | 0,02 | 0,00 |
| 122/ SLS- | -0,07 | -0,33 | -0,33 | -0,19 | -0,02 | -0,00 |
| 122/ SLS:CHR+ | 0,07 | 0,47 | 2,55 | 0,20 | 0,02 | 0,00 |
| 122/ SLS:CHR- | -0,07 | -0,33 | -0,33 | -0,19 | -0,02 | -0,00 |
| 122/ SLS:FRE+ | 0,01 | 0,04 | 1,05 | 0,07 | 0,00 | 0,00 |
| 122/ SLS:FRE- | -0,01 | -0,12 | 0,47 | -0,01 | -0,00 | -0,00 |
| 131/ 1 | -0,03 | -0,04 | 0,64 | 0,03 | 0,00 | -0,00 |
| 131/ 2 | 0,01 | -0,15 | 1,84 | 0,11 | 0,01 | -0,01 |
| 131/ 3 | -0,27 | -0,14 | -0,80 | 0,03 | -0,08 | 0,06 |
| 131/ 4 | 0,07 | -0,09 | -0,37 | 0,05 | 0,01 | 0,02 |
| 131/ 5 | 0,09 | -0,03 | -0,18 | 0,00 | 0,04 | 0,01 |
| 131/ 6 | 0,08 | 0,31 | -0,67 | -0,15 | 0,02 | -0,05 |
| 131/ ULS+ | 0,11 | 0,43 | 3,54 | 0,19 | 0,06 | 0,09 |
| 131/ ULS- | -0,43 | -0,28 | -0,56 | -0,20 | -0,12 | -0,08 |
| 131/ SLS+ | 0,06 | 0,27 | 2,49 | 0,13 | 0,04 | 0,06 |
| 131/ SLS- | -0,29 | -0,19 | -0,16 | -0,13 | -0,08 | -0,06 |
| 131/ SLS:CHR+ | 0,06 | 0,27 | 2,49 | 0,13 | 0,04 | 0,06 |
| 131/ SLS:CHR- | -0,29 | -0,19 | -0,16 | -0,13 | -0,08 | -0,06 |
| 131/ SLS:FRE+ | -0,01 | 0,02 | 1,01 | 0,05 | 0,01 | 0,01 |
| 131/ SLS:FRE- | -0,08 | -0,07 | 0,48 | -0,00 | -0,01 | -0,01 |
| 133/ 1 | 0,03 | -0,16 | 0,54 | -0,00 | 0,00 | 0,00 |
| 133/ 2 | 0,01 | -0,04 | 0,93 | -0,01 | 0,01 | 0,00 |
| 133/ 3 | -0,29 | -0,01 | -0,36 | 0,00 | -0,09 | -0,22 |
| 133/ 4 | 0,07 | -0,12 | -0,21 | 0,03 | 0,02 | 0,04 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|---------------|---------|---------|---------|----------|----------|----------|
| 133/ 5 | 0,11 | -0,00 | -0,06 | 0,00 | 0,04 | 0,04 |
| 133/ 6 | 0,08 | 0,16 | -0,46 | -0,03 | 0,02 | 0,11 |
| 133/ ULS+ | 0,21 | 0,08 | 2,04 | 0,05 | 0,06 | 0,16 |
| 133/ ULS- | -0,40 | -0,38 | -0,14 | -0,05 | -0,13 | -0,33 |
| 133/ SLS+ | 0,14 | -0,00 | 1,47 | 0,03 | 0,04 | 0,11 |
| 133/ SLS- | -0,25 | -0,28 | 0,09 | -0,04 | -0,09 | -0,22 |
| 133/ SLS:CHR+ | 0,14 | -0,00 | 1,47 | 0,03 | 0,04 | 0,11 |
| 133/ SLS:CHR- | -0,25 | -0,28 | 0,09 | -0,04 | -0,09 | -0,22 |
| 133/ SLS:FRE+ | 0,06 | -0,13 | 0,73 | 0,00 | 0,01 | 0,02 |
| 133/ SLS:FRE- | -0,02 | -0,18 | 0,45 | -0,01 | -0,02 | -0,04 |
| 140/ 1 | -0,02 | -0,04 | 0,63 | 0,03 | 0,00 | -0,00 |
| 140/ 2 | 0,00 | -0,18 | 1,81 | 0,13 | -0,00 | -0,00 |
| 140/ 3 | -0,02 | -0,01 | 0,06 | 0,00 | -0,02 | 0,00 |
| 140/ 4 | -0,00 | -0,09 | -0,49 | 0,04 | -0,00 | 0,03 |
| 140/ 5 | 0,02 | -0,03 | -0,27 | 0,01 | 0,02 | 0,01 |
| 140/ 6 | -0,00 | 0,32 | -0,81 | -0,18 | -0,00 | -0,04 |
| 140/ ULS+ | 0,01 | 0,44 | 3,46 | 0,23 | 0,03 | 0,04 |
| 140/ ULS- | -0,06 | -0,32 | -0,59 | -0,23 | -0,03 | -0,07 |
| 140/ SLS+ | 0,00 | 0,28 | 2,43 | 0,16 | 0,02 | 0,02 |
| 140/ SLS- | -0,04 | -0,22 | -0,18 | -0,15 | -0,02 | -0,05 |
| 140/ SLS:CHR+ | 0,00 | 0,28 | 2,43 | 0,16 | 0,02 | 0,02 |
| 140/ SLS:CHR- | -0,04 | -0,22 | -0,18 | -0,15 | -0,02 | -0,05 |
| 140/ SLS:FRE+ | -0,02 | 0,02 | 0,99 | 0,06 | 0,00 | 0,00 |
| 140/ SLS:FRE- | -0,03 | -0,08 | 0,47 | -0,00 | -0,00 | -0,01 |
| 146/ 1 | 0,03 | -0,04 | 0,64 | 0,03 | -0,00 | 0,00 |
| 146/ 2 | -0,01 | -0,16 | 1,86 | 0,11 | -0,01 | 0,01 |
| 146/ 3 | -0,05 | -0,02 | -0,02 | 0,01 | -0,03 | -0,00 |
| 146/ 4 | -0,10 | -0,10 | -0,46 | 0,05 | -0,03 | -0,02 |
| 146/ 5 | 0,25 | -0,15 | -0,79 | 0,04 | 0,08 | -0,06 |
| 146/ 6 | -0,09 | 0,33 | -0,71 | -0,17 | -0,02 | 0,06 |
| 146/ ULS+ | 0,41 | 0,46 | 3,56 | 0,20 | 0,11 | 0,08 |
| 146/ ULS- | -0,12 | -0,28 | -0,54 | -0,23 | -0,04 | -0,09 |
| 146/ SLS+ | 0,28 | 0,29 | 2,50 | 0,14 | 0,07 | 0,06 |
| 146/ SLS- | -0,07 | -0,20 | -0,14 | -0,14 | -0,03 | -0,06 |
| 146/ SLS:CHR+ | 0,28 | 0,29 | 2,50 | 0,14 | 0,07 | 0,06 |
| 146/ SLS:CHR- | -0,07 | -0,20 | -0,14 | -0,14 | -0,03 | -0,06 |
| 146/ SLS:FRE+ | 0,08 | 0,03 | 1,01 | 0,05 | 0,01 | 0,01 |
| 146/ SLS:FRE- | 0,01 | -0,07 | 0,49 | -0,01 | -0,01 | -0,01 |
| 148/ 1 | -0,03 | -0,16 | 0,54 | -0,00 | -0,00 | -0,00 |
| 148/ 2 | -0,01 | -0,05 | 0,93 | -0,00 | -0,01 | -0,00 |
| 148/ 3 | -0,07 | 0,00 | 0,03 | -0,00 | -0,03 | -0,01 |
| 148/ 4 | -0,10 | -0,13 | -0,25 | 0,03 | -0,03 | -0,05 |
| 148/ 5 | 0,27 | -0,05 | -0,35 | 0,02 | 0,09 | 0,21 |
| 148/ 6 | -0,09 | 0,19 | -0,49 | -0,04 | -0,03 | -0,12 |
| 148/ ULS+ | 0,37 | 0,13 | 2,04 | 0,05 | 0,13 | 0,31 |
| 148/ ULS- | -0,19 | -0,39 | -0,19 | -0,06 | -0,05 | -0,18 |
| 148/ SLS+ | 0,24 | 0,03 | 1,47 | 0,03 | 0,08 | 0,20 |
| 148/ SLS- | -0,14 | -0,29 | 0,05 | -0,04 | -0,03 | -0,12 |
| 148/ SLS:CHR+ | 0,24 | 0,03 | 1,47 | 0,03 | 0,08 | 0,20 |
| 148/ SLS:CHR- | -0,14 | -0,29 | 0,05 | -0,04 | -0,03 | -0,12 |
| 148/ SLS:FRE+ | 0,02 | -0,12 | 0,73 | 0,00 | 0,01 | 0,04 |
| 148/ SLS:FRE- | -0,05 | -0,19 | 0,44 | -0,01 | -0,01 | -0,02 |
| Case 1 | DL1 | | | | | |
| Sum of val. | 0,00 | 0,00 | 30,41 | 0,02 | -0,00 | 0,00 |
| Sum of reac. | 0,00 | 0,00 | 30,41 | 266,86 | -156,64 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -30,41 | -266,86 | 156,64 | 0,00 |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|------------------|---|-------------|---------|----------|----------|----------|
| Check val. | 0,00 | 0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 5,92810e-14 | 1,00078e-15 | | | | |
| Case 2 | SN1 | | | | | |
| Sum of val. | -0,00 | -0,00 | 88,53 | 0,09 | -0,01 | 0,00 |
| Sum of reac. | -0,00 | -0,00 | 88,53 | 784,11 | -457,08 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -88,53 | -784,11 | 457,08 | -0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 4,88788e-14 | 7,49713e-16 | | | | |
| Case 3 | Wind X+ 28,06 m/s (f=1.00) S- imulation | | | | | |
| Sum of val. | -8,04 | 0,49 | -11,26 | -0,23 | -3,04 | -0,00 |
| Sum of reac. | -8,04 | 0,49 | -11,26 | -89,30 | 9,05 | 65,58 |
| Sum of forc. | 8,04 | -0,49 | 11,26 | 89,30 | -9,05 | -65,58 |
| Check val. | 0,00 | -0,00 | -0,00 | -0,00 | -0,00 | 0,00 |
| Precision | 1,60461e-13 | 4,04332e-17 | | | | |
| Case 4 | Wind Y+ 28,06 m/s (f=1.00) S- imulation | | | | | |
| Sum of val. | 0,06 | -4,65 | -24,75 | 2,09 | -0,19 | -0,01 |
| Sum of reac. | 0,06 | -4,65 | -24,75 | -212,48 | 133,36 | -19,99 |
| Sum of forc. | -0,06 | 4,65 | 24,75 | 212,48 | -133,36 | 19,99 |
| Check val. | -0,00 | 0,00 | -0,00 | -0,00 | 0,00 | -0,00 |
| Precision | 7,87094e-14 | 9,47370e-16 | | | | |
| Case 5 | Wind X- 28,06 m/s (f=1.00) S- imulation | | | | | |
| Sum of val. | 7,92 | -0,38 | -15,32 | 0,16 | 2,97 | -0,01 |
| Sum of reac. | 7,92 | -0,38 | -15,32 | -141,92 | 113,96 | -71,06 |
| Sum of forc. | -7,92 | 0,38 | 15,32 | 141,92 | -113,96 | 71,06 |
| Check val. | -0,00 | 0,00 | 0,00 | -0,00 | 0,00 | -0,00 |
| Precision | 1,68315e-13 | 2,62787e-15 | | | | |
| Case 6 | Wind Y- 28,06 m/s (f=1.00) S- imulation | | | | | |
| Sum of val. | -0,26 | 5,12 | -29,45 | -2,41 | -0,14 | 0,02 |
| Sum of reac. | -0,26 | 5,12 | -29,45 | -276,19 | 155,60 | 31,46 |
| Sum of forc. | 0,26 | -5,12 | 29,45 | 276,19 | -155,60 | -31,46 |
| Check val. | 0,00 | -0,00 | -0,00 | -0,00 | 0,00 | 0,00 |
| Precision | 9,43780e-14 | 7,32820e-16 | | | | |
| Case ULS+ | ULS+ | | | | | |
| Sum of val. | 32,82 | 8,31 | 169,34 | 3,76 | 18,86 | 1,79 |
| Sum of reac. | -0,00 | -0,00 | 163,21 | 1443,03 | -842,26 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -163,21 | -1443,03 | 842,26 | -0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 1,32599e-13 | 2,12535e-15 | | | | |
| Case ULS- | ULS- | | | | | |
| Sum of val. | -32,77 | -7,76 | -19,19 | -3,94 | -18,46 | -1,90 |
| Sum of reac. | -0,00 | -0,00 | 163,21 | 1443,03 | -842,26 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -163,21 | -1443,03 | 842,26 | -0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 1,32599e-13 | 2,12535e-15 | | | | |

| Node/Case | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|----------------------|-------------|-------------|---------|----------|----------|----------|
| Case SLS+ | SLS+ | | | | | |
| Sum of val. | 21,45 | 5,41 | 118,94 | 2,49 | 12,30 | 1,19 |
| Sum of reac. | 0,00 | 0,00 | 30,41 | 266,86 | -156,64 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -30,41 | -266,86 | 156,64 | 0,00 |
| Check val. | 0,00 | 0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 5,92810e-14 | 1,00078e-15 | | | | |
| Case SLS- | SLS- | | | | | |
| Sum of val. | -21,41 | -5,04 | -2,66 | -2,60 | -12,03 | -1,26 |
| Sum of reac. | 0,00 | 0,00 | 30,41 | 266,86 | -156,64 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -30,41 | -266,86 | 156,64 | 0,00 |
| Check val. | 0,00 | 0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 5,92810e-14 | 1,00078e-15 | | | | |
| Case SLS:CHR+ | SLS:CHR+ | | | | | |
| Sum of val. | 21,45 | 5,41 | 118,94 | 2,49 | 12,30 | 1,19 |
| Sum of reac. | -0,00 | -0,00 | 118,94 | 1050,97 | -613,72 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -118,94 | -1050,97 | 613,72 | -0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 1,08160e-13 | 1,75050e-15 | | | | |
| Case SLS:CHR- | SLS:CHR- | | | | | |
| Sum of val. | -21,41 | -5,04 | -2,66 | -2,60 | -12,03 | -1,26 |
| Sum of reac. | -0,00 | -0,00 | 118,94 | 1050,97 | -613,72 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -118,94 | -1050,97 | 613,72 | -0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 1,08160e-13 | 1,75050e-15 | | | | |
| Case SLS:FRE+ | SLS:FRE+ | | | | | |
| Sum of val. | 4,29 | 1,08 | 48,12 | 0,52 | 2,46 | 0,24 |
| Sum of reac. | -0,00 | -0,00 | 48,12 | 423,69 | -248,05 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -48,12 | -423,69 | 248,05 | 0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 6,90567e-14 | 1,15073e-15 | | | | |
| Case SLS:FRE- | SLS:FRE- | | | | | |
| Sum of val. | -4,28 | -1,01 | 23,80 | -0,50 | -2,41 | -0,25 |
| Sum of reac. | -0,00 | -0,00 | 48,12 | 423,69 | -248,05 | -0,00 |
| Sum of forc. | -0,00 | -0,00 | -48,12 | -423,69 | 248,05 | 0,00 |
| Check val. | -0,00 | -0,00 | 0,00 | 0,00 | -0,00 | -0,00 |
| Precision | 6,90567e-14 | 1,15073e-15 | | | | |

6.12 Reactions ULS: Global extremes

| | FX (kN) | FY (kN) | FZ (kN) | MX (kNm) | MY (kNm) | MZ (kNm) |
|-------------|---------|---------|---------|----------|----------|----------|
| MAX | 10,22 | 0,74 | 24,62 | 0,31 | 6,91 | 0,33 |
| Node | 99 | 122 | 106 | 106 | 99 | 14 |
| Case | ULS/13 | ULS/12 | ULS/13 | ULS/10 | ULS/13 | ULS/5 |
| MIN | -10,06 | -0,73 | -4,61 | -0,37 | -6,83 | -0,33 |
| Node | 112 | 24 | 106 | 77 | 112 | 133 |
| Case | ULS/13 | ULS/6 | 6 | ULS/12 | ULS/13 | ULS/9 |

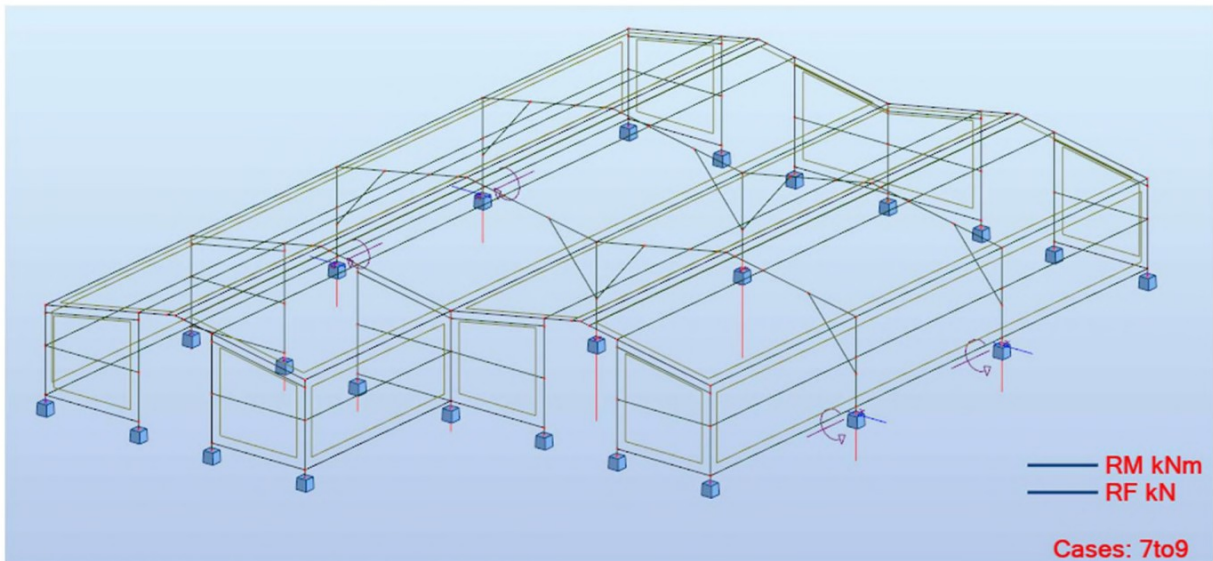


Figure shows reactions in all supports

6.13 Stresses – Global extremes

| | S max (MPa) | S min (MPa) | S max(My) (MPa) | S max(Mz) (MPa) | S min(My) (MPa) | S min(Mz) (MPa) | Fx/Ax (MPa) |
|---------------|-------------|-------------|-----------------|-----------------|-----------------|-----------------|-------------|
| MAX | 284,93 | 26,96 | 176,89 | 237,04 | -0,00 | -0,00 | 60,58 |
| Member | 102 | 5 | 102 | 97 | 19 | 125 | 77 |
| Node | 23 | 22 | 23 | 40 | 122 | 25 | 94 |
| Case | ULS/13 | ULS/13 | ULS/13 | ULS/9 | SLS/12 | SLS/3 | ULS/13 |
| MIN | -7,51 | -220,43 | 0,00 | 0,00 | -176,89 | -199,44 | -11,63 |
| Member | 74 | 102 | 19 | 125 | 102 | 126 | 76 |
| Node | 64 | 23 | 122 | 25 | 23 | 103 | 85 |
| Case | 3 | ULS/13 | SLS/12 | SLS/3 | ULS/13 | ULS/13 | 5 |

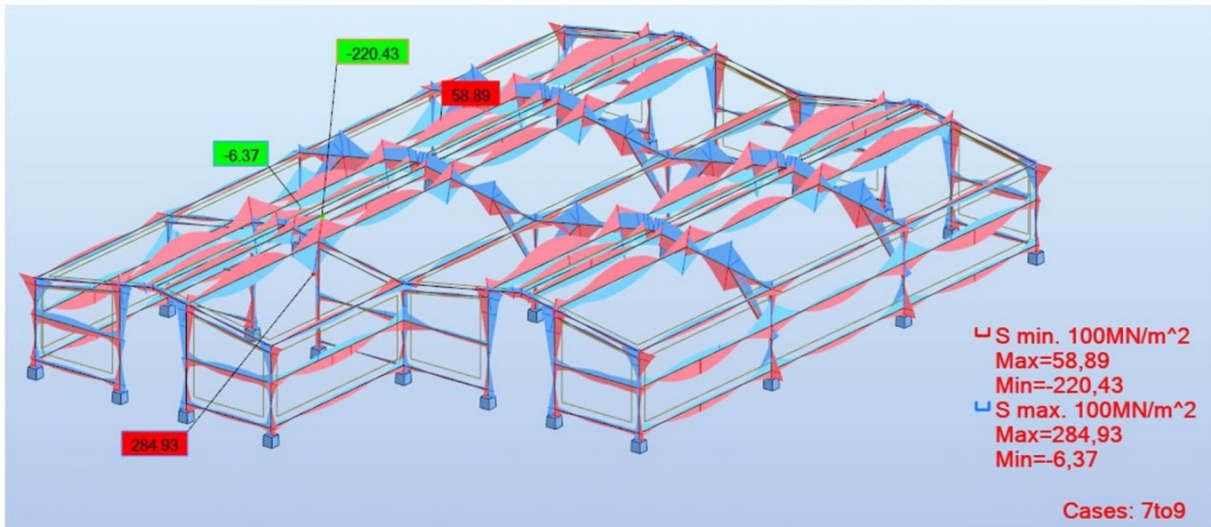


Figure shows global extremes of stresses (S_{max} and S_{min})

6.14 Displacement SLS: Global extremes

| | UX (cm) | UY (cm) | UZ (cm) | RX (Rad) | RY (Rad) | RZ (Rad) |
|-------------|---------|---------|---------|----------|----------|----------|
| MAX | 0,4 | 0,3 | 0,3 | 0,011 | 0,009 | 0,011 |
| Node | 113 | 127 | 82 | 123 | 97 | 119 |
| Case | SLS/6 | SLS/6 | 6 | SLS/6 | SLS/6 | 3 |
| MIN | -0,4 | -0,3 | -1,1 | -0,010 | -0,009 | -0,011 |
| Node | 93 | 144 | 105 | 44 | 115 | 19 |
| Case | SLS/6 | 6 | SLS/6 | SLS/6 | SLS/6 | SLS/2 |

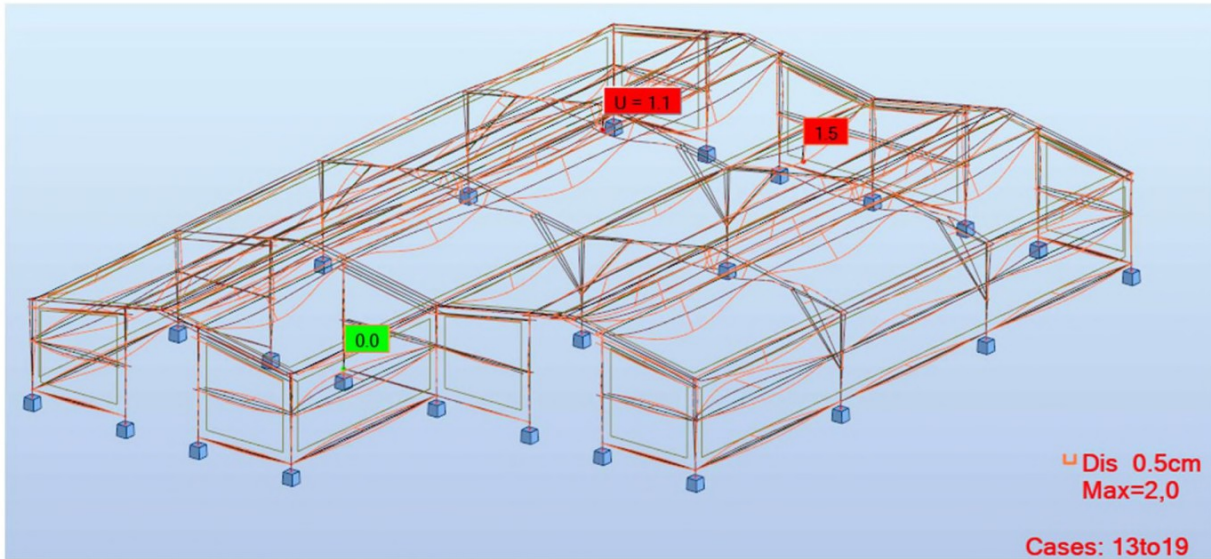


Figure shows displacement SLS for bars

6.15 Members – Definition

| Member | Name | Components | Code group | Section | Type | Ly (m) | Lz (m) |
|--------|-----------|------------|------------|-----------|--------|--------|--------|
| 1 | Column_1 | 1 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 2 | Column_2 | 2 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 3 | Column_3 | 3 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 4 | Column_4 | 4 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 5 | Column_5 | 5 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 6 | Column_6 | 6 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 7 | Column_7 | 7 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 8 | Column_8 | 8 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 9 | Column_9 | 9 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 10 | Column_10 | 10 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 11 | Column_11 | 11 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 12 | Column_12 | 12 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 13 | Column_13 | 13 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 14 | Column_14 | 14 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 15 | Column_15 | 15 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 16 | Column_16 | 16 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 17 | Column_17 | 17 | Columns | IPE 120 | Column | 1,77 | 1,77 |
| 18 | Column_18 | 18 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 19 | Column_19 | 19 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 20 | Column_20 | 20 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 21 | Column_21 | 21 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 22 | Column_22 | 22 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 23 | Column_23 | 23 | Columns | K 40x40x2 | Column | 2,12 | 2,12 |
| 24 | Column_24 | 24 | Columns | K 40x40x2 | Column | 1,77 | 1,77 |
| 25 | Beam_25 | 25 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 26 | Beam_26 | 26 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 27 | Beam_27 | 27 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 28 | Beam_28 | 28 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 29 | Beam_29 | 29 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 30 | Beam_30 | 30 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 31 | Beam_31 | 31 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 32 | Beam_32 | 32 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 33 | Beam_33 | 33 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 34 | Beam_34 | 34 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 35 | Beam_35 | 35 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 36 | Beam_36 | 36 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 37 | Beam_37 | 37 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 38 | Beam_38 | 38 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 39 | Beam_39 | 39 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 40 | Beam_40 | 40 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 41 | Beam_41 | 41 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 42 | Beam_42 | 42 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 43 | Beam_43 | 43 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 44 | Beam_44 | 44 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 45 | Beam_45 | 45 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 46 | Beam_46 | 46 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 47 | Beam_47 | 47 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 48 | Beam_48 | 48 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 49 | Beam_49 | 49 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 50 | Beam_50 | 50 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 51 | Beam_51 | 51 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 52 | Beam_52 | 52 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 53 | Beam_53 | 53 | Wall beams | K 40x20x2 | Beam | 2,00 | 2,00 |
| 54 | Beam_54 | 54 | Wall beams | K 40x20x2 | Beam | 2,03 | 2,03 |
| 55 | Beam_55 | 55 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 56 | Beam_56 | 56 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |

| Member | Name | Components | Code group | Section | Type | Ly (m) | Lz (m) |
|--------|----------|------------|------------|--------------|------|--------|--------|
| 57 | Beam_57 | 57 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 58 | Beam_58 | 58 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 59 | Beam_59 | 59 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 60 | Beam_60 | 60 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 61 | Beam_61 | 61 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 62 | Beam_62 | 62 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 63 | Beam_63 | 63 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 64 | Beam_64 | 64 | Roof beams | K 80x40x3 | Beam | 2,82 | 2,82 |
| 65 | Beam_65 | 65 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 66 | Beam_66 | 66 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 67 | Beam_67 | 67 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 68 | Beam_68 | 68 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 69 | Beam_69 | 69 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 70 | Beam_70 | 70 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 71 | Beam_71 | 71 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 72 | Beam_72 | 72 | Roof beams | K 70x50x4 | Beam | 2,82 | 2,82 |
| 73 | Beam_73 | 73 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 74 | Beam_74 | 74 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 75 | Beam_75 | 75 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 76 | Beam_76 | 76 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 77 | Beam_77 | 77 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 78 | Beam_78 | 78 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 79 | Beam_79 | 79 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 80 | Beam_80 | 80 | Struts | K 40x40x2 | Beam | 1,59 | 1,59 |
| 81 | Beam_81 | 81 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 82 | Beam_82 | 82 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 83 | Beam_83 | 83 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 84 | Beam_84 | 84 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 85 | Beam_85 | 85 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 86 | Beam_86 | 86 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 87 | Beam_87 | 87 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 88 | Beam_88 | 88 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 89 | Beam_89 | 89 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 90 | Beam_90 | 90 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 91 | Beam_91 | 91 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 92 | Beam_92 | 92 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 93 | Beam_93 | 93 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 94 | Beam_94 | 94 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 95 | Beam_95 | 95 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 96 | Beam_96 | 96 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 97 | Beam_97 | 97 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 98 | Beam_98 | 98 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 99 | Beam_99 | 99 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 100 | Beam_100 | 100 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 101 | Beam_101 | 101 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 102 | Beam_102 | 102 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 103 | Beam_103 | 103 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 104 | Beam_104 | 104 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 105 | Beam_105 | 105 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 106 | Beam_106 | 106 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 107 | Beam_107 | 107 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 108 | Beam_108 | 108 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 109 | Beam_109 | 109 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 110 | Beam_110 | 110 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 111 | Beam_111 | 111 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 112 | Beam_112 | 112 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 113 | Beam_113 | 113 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |

| Member | Name | Components | Code group | Section | Type | Ly (m) | Lz (m) |
|--------|----------|------------|------------|---------------|------|--------|--------|
| 114 | Beam_114 | 114 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 115 | Beam_115 | 115 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 116 | Beam_116 | 116 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 117 | Beam_117 | 117 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 118 | Beam_118 | 118 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 119 | Beam_119 | 119 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 120 | Beam_120 | 120 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 121 | Beam_121 | 121 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 122 | Beam_122 | 122 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 123 | Beam_123 | 123 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 124 | Beam_124 | 124 | Purlins | TELG 80x40x3 | Beam | 4,00 | 4,00 |
| 125 | Beam_125 | 125 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 126 | Beam_126 | 126 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 127 | Beam_127 | 127 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 128 | Beam_128 | 128 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 129 | Beam_129 | 129 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 130 | Beam_130 | 130 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 131 | Beam_131 | 131 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 132 | Beam_132 | 132 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 133 | Beam_133 | 133 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 134 | Beam_134 | 134 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |
| 135 | Beam_135 | 135 | Gutters | TELG 100x65x3 | Beam | 4,00 | 4,00 |

6.16 Members – Code groups

| Code group | Name | Components |
|------------|------------|------------|
| 1 | Columns | 1to24 |
| 2 | Wall beams | 25to54 |
| 3 | Roof beams | 55to72 |
| 4 | Struts | 73to80 |
| 5 | Purlins | 81to124 |
| 6 | Gutters | 125to135 |

6.17 Member Verification summary

| Member | Section | Material | Lay | Laz | Ratio | Case |
|----------------------------------|----------------|----------|--------|--------|-------|------------|
| Code group : 1 Columns | | | | | | |
| 19 Column_19 | OK K 40x40x2 | S235 | 113.86 | 113.86 | 0.65 | 7 ULS /13/ |
| Code group : 2 Wall beams | | | | | | |
| 42 Beam_42 | OK K 40x20x2 | S235 | 141.82 | 249.38 | 0.26 | 7 ULS /10/ |
| Code group : 3 Roof beams | | | | | | |
| 67 Beam_67 | OK K 70x50x4 | S235 | 109.55 | 143.58 | 0.80 | 7 ULS /13/ |
| Code group : 4 Struts | | | | | | |
| 77 Beam_77 | OK K 40x40x2 | S235 | 102.65 | 102.65 | 0.55 | 7 ULS /13/ |
| Code group : 5 Purlins | | | | | | |
| 102 Beam_102 | OK TELG 80x40x | S235 | 127.89 | 320.26 | 0.90 | 7 ULS /13/ |
| Code group : 6 Gutters | | | | | | |
| 126 Beam_126 | OK TELG 100x65 | S235 | 82.56 | 160.52 | 0.64 | 7 ULS /13/ |

Member verification in ULS

Conclusion → **All sections OK !!!**

Paragraph 6.18 shows the full member verification in ULS of the highlighted bars from this summary. The full member verification of all members is available upon request.

6.18 Member Verification

STEEL DESIGN

CODE: NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 1 Columns

MEMBER: 19 Column_19
0.00 m

POINT: 1

COORDINATE: x = 0.00 L =

LOADS:

Governing Load Case: 7 ULS /13/ 1*1.20 + 2*1.50

MATERIAL:

S235 (S235) fy = 235.00 MPa



SECTION PARAMETERS: K 40x40x2

| | | | |
|-----------|---------------------------|---------------------------|--------------------------|
| h=4.0 cm | gM0=1.00 | gM1=1.00 | |
| b=4.0 cm | Ay=1.44 cm ² | Az=1.44 cm ² | Ax=3.04 cm ² |
| tw=0.2 cm | Iy=7.34 cm ⁴ | Iz=7.34 cm ⁴ | Ix=11.01 cm ⁴ |
| tf=0.2 cm | Wply=4.34 cm ³ | Wplz=4.34 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|------------------|------------------------|------------------------|----------------------|
| N,Ed = 3.63 kN | My,Ed = -0.00 kN*m | Mz,Ed = 0.29 kN*m | Vy,Ed = 0.48 kN |
| Nc,Rd = 71.44 kN | My,Ed,max = -0.00 kN*m | Mz,Ed,max = -0.58 kN*m | Vy,T,Rd = 19.53 kN |
| Nb,Rd = 37.31 kN | My,c,Rd = 1.02 kN*m | Mz,c,Rd = 1.02 kN*m | Vz,Ed = 0.00 kN |
| | MN,y,Rd = 1.02 kN*m | MN,z,Rd = 1.02 kN*m | Vz,T,Rd = 19.53 kN |
| | | | Tt,Ed = -0.00 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About y axis:

| | |
|----------------|--------------|
| Ly = 1.77 m | Lam_y = 1.21 |
| Lcr,y = 1.77 m | Xy = 0.52 |
| Lamy = 113.86 | kzy = 0.58 |



About z axis:

| | |
|----------------|--------------|
| Lz = 1.77 m | Lam_z = 1.21 |
| Lcr,z = 1.77 m | Xz = 0.52 |
| Lamz = 113.86 | kzz = 0.97 |

VERIFICATION FORMULAS:

Section strength check:

- N,Ed/Nc,Rd = 0.05 < 1.00 (6.2.4.(1))
- My,Ed/MN,y,Rd = 0.00 < 1.00 (6.2.9.1.(2))
- Mz,Ed/MN,z,Rd = 0.28 < 1.00 (6.2.9.1.(2))
- (My,Ed/MN,y,Rd)^1.66 + (Mz,Ed/MN,z,Rd)^1.66 = 0.12 < 1.00 (6.2.9.1.(6))
- 1.00*(My,Ed/MN,y,Rd)^1.00 + 0.75*(Mz,Ed/MN,z,Rd)^2.00 = 0.06 < 1.00 (6.2.10.(7))
- Vy,Ed/Vy,T,Rd = 0.02 < 1.00 (6.2.6-7)
- Vz,Ed/Vz,T,Rd = 0.00 < 1.00 (6.2.6-7)
- Tau,ty,Ed/(fy/(sqrt(3)*gM0)) = 0.00 < 1.00 (6.2.6)
- Tau,tz,Ed/(fy/(sqrt(3)*gM0)) = 0.00 < 1.00 (6.2.6)

Global stability check of member:

- Lambda,y = 113.86 < Lambda,max = 210.00 Lambda,z = 113.86 < Lambda,max = 210.00 STABLE
- N,Ed/(Xy*N,Rk/gM1) + kyy*My,Ed,max/(XLT*My,Rk/gM1) + kyz*Mz,Ed,max/(Mz,Rk/gM1) = 0.43 < 1.00 (6.3.3.(4))
- N,Ed/(Xz*N,Rk/gM1) + kzy*My,Ed,max/(XLT*My,Rk/gM1) + kzz*Mz,Ed,max/(Mz,Rk/gM1) = 0.65 < 1.00 (6.3.3.(4))

Section OK !!!

STEEL DESIGN

CODE: NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 2 Wall beams

MEMBER: 42 Beam_42

POINT: 3

COORDINATE: x = 1.00 L =

2.00 m

LOADS:

Governing Load Case: 7 ULS /10/ 1*1.00 + 4*1.50

MATERIAL:

S235 (S235) $f_y = 235.00$ MPa



SECTION PARAMETERS: K 40x20x2

| | | | |
|-----------|---------------------------|---------------------------|-------------------------|
| h=4.0 cm | gM0=1.00 | gM1=1.00 | |
| b=2.0 cm | Ay=0.64 cm ² | Az=1.44 cm ² | Ax=2.24 cm ² |
| tw=0.2 cm | Iy=4.45 cm ⁴ | Iz=1.44 cm ⁴ | Ix=3.37 cm ⁴ |
| tf=0.2 cm | Wply=2.82 cm ³ | Wplz=1.70 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|---------------------------|----------------------------------|-----------------------------------|-------------------------------|
| N _{Ed} = 0.07 kN | My _{Ed} = 0.02 kN*m | Mz _{Ed} = -0.10 kN*m | Vy _{Ed} = 0.29 kN |
| Nc,Rd = 52.64 kN | My _{Ed,max} = 0.02 kN*m | Mz _{Ed,max} = -0.10 kN*m | Vy,T,Rd = 8.63 kN |
| Nb,Rd = 52.64 kN | My,c,Rd = 0.66 kN*m | Mz,c,Rd = 0.40 kN*m | Vz _{Ed} = 0.01 kN |
| | MN _{y,Rd} = 0.66 kN*m | MN _{z,Rd} = 0.40 kN*m | Vz,T,Rd = 19.41 kN |
| | Mb,Rd = 0.66 kN*m | | Tt _{Ed} = -0.00 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

| | | | |
|----------------|-----------------|--------------|----------------|
| z = 1.00 | Mcr = 5.03 kN*m | Curve,LT - d | XLT = 1.00 |
| Lcr,upp=2.00 m | Lam_LT = 0.36 | fi,LT = 0.54 | XLT,mod = 1.00 |

BUCKLING PARAMETERS:



About y axis:

$k_{zy} = 0.54$



About z axis:

$k_{zz} = 0.90$

VERIFICATION FORMULAS:

Section strength check:

$N_{Ed}/N_{c,Rd} = 0.00 < 1.00$ (6.2.4.(1))
 $M_{y,Ed}/M_{N,y,Rd} = 0.03 < 1.00$ (6.2.9.1.(2))
 $M_{z,Ed}/M_{N,z,Rd} = 0.26 < 1.00$ (6.2.9.1.(2))
 $(M_{y,Ed}/M_{N,y,Rd})^{1.66} + (M_{z,Ed}/M_{N,z,Rd})^{1.66} = 0.11 < 1.00$ (6.2.9.1.(6))
 $1.00*(M_{y,Ed}/M_{N,y,Rd})^{1.00} + 0.75*(M_{z,Ed}/M_{N,z,Rd})^{2.00} = 0.08 < 1.00$ (6.2.10.(7))
 $V_{y,Ed}/V_{y,T,Rd} = 0.03 < 1.00$ (6.2.6-7)
 $V_{z,Ed}/V_{z,T,Rd} = 0.00 < 1.00$ (6.2.6-7)
 $\tau_{ty,Ed}/(f_y/(\sqrt{3})*gM0) = 0.01 < 1.00$ (6.2.6)
 $\tau_{tz,Ed}/(f_y/(\sqrt{3})*gM0) = 0.01 < 1.00$ (6.2.6)

Global stability check of member:

$M_{y,Ed,max}/M_{b,Rd} = 0.03 < 1.00$ (6.3.2.1.(1))
 $N_{Ed}/(X_y*N_{Rk}/gM1) + k_{yy}*M_{y,Ed,max}/(XLT*M_{y,Rk}/gM1) + k_{yz}*M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.17 < 1.00$ (6.3.3.(4))
 $N_{Ed}/(X_z*N_{Rk}/gM1) + k_{zy}*M_{y,Ed,max}/(XLT*M_{y,Rk}/gM1) + k_{zz}*M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.25 < 1.00$ (6.3.3.(4))

Section OK !!!

STEEL DESIGN

CODE: NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 3 Roof beams

MEMBER: 67 Beam_67

POINT: 3

COORDINATE: x = 0.63 L =

1.78 m

LOADS:

Governing Load Case: 7 ULS /13/ 1*1.20 + 2*1.50

MATERIAL:

S235 (S235) $f_y = 235.00$ MPa



SECTION PARAMETERS: K 70x50x4

| | | | |
|-----------|----------------------------|----------------------------|--------------------------|
| h=7.0 cm | gM0=1.00 | gM1=1.00 | |
| b=5.0 cm | Ay=3.36 cm ² | Az=4.96 cm ² | Ax=8.96 cm ² |
| tw=0.4 cm | Iy=59.50 cm ⁴ | Iz=34.64 cm ⁴ | Ix=66.32 cm ⁴ |
| tf=0.4 cm | Wply=20.89 cm ³ | Wplz=16.41 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|----------------------------|-----------------------------------|----------------------------------|------------------------------|
| N _{Ed} = 11.65 kN | My _{Ed} = -3.91 kN*m | Mz _{Ed} = 0.02 kN*m | Vy _{Ed} = -0.04 kN |
| Nc,Rd = 210.56 kN | My _{Ed,max} = -3.91 kN*m | Mz _{Ed,max} = 0.06 kN*m | Vy,T,Rd = 45.35 kN |
| Nb,Rd = 210.56 kN | My,c,Rd = 4.91 kN*m | Mz,c,Rd = 3.86 kN*m | Vz _{Ed} = -6.23 kN |
| | MN _{y,Rd} = 4.91 kN*m | MN _{z,Rd} = 3.86 kN*m | Vz,T,Rd = 66.94 kN |
| | Mb,Rd = 4.91 kN*m | | Tt _{Ed} = 0.02 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

| | | | |
|----------------|------------------|--------------|----------------|
| z = 1.00 | Mcr = 77.01 kN*m | Curve,LT - d | XLT = 1.00 |
| Lcr,low=2.82 m | Lam_LT = 0.25 | fi,LT = 0.47 | XLT,mod = 1.00 |

BUCKLING PARAMETERS:



About y axis:

$$k_{yy} = 0.90$$



About z axis:

$$k_{yz} = 0.54$$

VERIFICATION FORMULAS:

Section strength check:

$$N_{Ed}/N_{c,Rd} = 0.06 < 1.00 \quad (6.2.4.(1))$$

$$M_{y,Ed}/M_{N,y,Rd} = 0.80 < 1.00 \quad (6.2.9.1.(2))$$

$$M_{z,Ed}/M_{N,z,Rd} = 0.00 < 1.00 \quad (6.2.9.1.(2))$$

$$(M_{y,Ed}/M_{N,y,Rd})^{1.67} + (M_{z,Ed}/M_{N,z,Rd})^{1.67} = 0.68 < 1.00 \quad (6.2.9.1.(6))$$

$$1.00 * (M_{y,Ed}/M_{N,y,Rd})^{1.00} + 0.75 * (M_{z,Ed}/M_{N,z,Rd})^{2.00} = 0.80 < 1.00 \quad (6.2.10.(7))$$

$$V_{y,Ed}/V_{y,T,Rd} = 0.00 < 1.00 \quad (6.2.6-7)$$

$$V_{z,Ed}/V_{z,T,Rd} = 0.09 < 1.00 \quad (6.2.6-7)$$

$$\tau_{ty,Ed}/(f_y/(\sqrt{3}) * gM0) = 0.01 < 1.00 \quad (6.2.6)$$

$$\tau_{tz,Ed}/(f_y/(\sqrt{3}) * gM0) = 0.01 < 1.00 \quad (6.2.6)$$

Global stability check of member:

$$M_{y,Ed,max}/M_{b,Rd} = 0.80 < 1.00 \quad (6.3.2.1.(1))$$

$$N_{Ed}/(X_y * N_{Rk}/gM1) + k_{yy} * M_{y,Ed,max}/(XLT * M_{y,Rk}/gM1) + k_{yz} * M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.78 < 1.00 \quad (6.3.3.(4))$$

$$N_{Ed}/(X_z * N_{Rk}/gM1) + k_{zy} * M_{y,Ed,max}/(XLT * M_{y,Rk}/gM1) + k_{zz} * M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.50 < 1.00 \quad (6.3.3.(4))$$

Section OK !!!

STEEL DESIGN

CODE: NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 4 Struts

MEMBER: 77 Beam_77

POINT: 2

COORDINATE: x = 0.50 L =

0.80 m

LOADS:

Governing Load Case: 7 ULS /13/ 1*1.20 + 2*1.50

MATERIAL:

S235 (S235) $f_y = 235.00$ MPa



SECTION PARAMETERS: K 40x40x2

| | | | |
|-----------|---------------------------|---------------------------|--------------------------|
| h=4.0 cm | gM0=1.00 | gM1=1.00 | |
| b=4.0 cm | Ay=1.44 cm ² | Az=1.44 cm ² | Ax=3.04 cm ² |
| tw=0.2 cm | Iy=7.34 cm ⁴ | Iz=7.34 cm ⁴ | Ix=11.01 cm ⁴ |
| tf=0.2 cm | Wply=4.34 cm ³ | Wplz=4.34 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|----------------------------|-----------------------------------|----------------------------------|------------------------------|
| N _{Ed} = 18.40 kN | My _{Ed} = -0.08 kN*m | Mz _{Ed} = 0.01 kN*m | Vy _{Ed} = 0.02 kN |
| Nc,Rd = 71.44 kN | My _{Ed,max} = -0.31 kN*m | Mz _{Ed,max} = 0.02 kN*m | Vy,T,Rd = 19.49 kN |
| Nb,Rd = 71.44 kN | My,c,Rd = 1.02 kN*m | Mz,c,Rd = 1.02 kN*m | Vz _{Ed} = 0.28 kN |
| | MN _{y,Rd} = 0.99 kN*m | MN _{z,Rd} = 0.99 kN*m | Vz,T,Rd = 19.49 kN |
| | Mb,Rd = 1.02 kN*m | | Tt _{Ed} = 0.00 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

| | | | |
|----------------|------------------|--------------|----------------|
| z = 1.00 | Mcr = 25.50 kN*m | Curve,LT - d | XLT = 1.00 |
| Lcr,low=1.59 m | Lam_LT = 0.20 | fi,LT = 0.44 | XLT,mod = 1.00 |

BUCKLING PARAMETERS:



About y axis:

$k_{yy} = 0.90$



About z axis:

$k_{yz} = 0.54$

VERIFICATION FORMULAS:

Section strength check:

$N_{Ed}/N_{c,Rd} = 0.26 < 1.00$ (6.2.4.(1))
 $M_{y,Ed}/M_{N,y,Rd} = 0.08 < 1.00$ (6.2.9.1.(2))
 $M_{z,Ed}/M_{N,z,Rd} = 0.01 < 1.00$ (6.2.9.1.(2))
 $(M_{y,Ed}/M_{N,y,Rd})^{1.79} + (M_{z,Ed}/M_{N,z,Rd})^{1.79} = 0.01 < 1.00$ (6.2.9.1.(6))
 $1.00 \cdot (M_{y,Ed}/M_{N,y,Rd})^{1.00} + 0.75 \cdot (M_{z,Ed}/M_{N,z,Rd})^{2.00} = 0.08 < 1.00$ (6.2.10.(7))
 $V_{y,Ed}/V_{y,T,Rd} = 0.00 < 1.00$ (6.2.6-7)
 $V_{z,Ed}/V_{z,T,Rd} = 0.01 < 1.00$ (6.2.6-7)
 $\tau_{ty,Ed}/(f_y/(\sqrt{3}) \cdot gM0) = 0.00 < 1.00$ (6.2.6)
 $\tau_{tz,Ed}/(f_y/(\sqrt{3}) \cdot gM0) = 0.00 < 1.00$ (6.2.6)

Global stability check of member:

$M_{y,Ed,max}/M_{b,Rd} = 0.31 < 1.00$ (6.3.2.1.(1))
 $N_{Ed}/(X_y \cdot N_{Rk}/gM1) + k_{yy} \cdot M_{y,Ed,max}/(XLT \cdot M_{y,Rk}/gM1) + k_{yz} \cdot M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.55 < 1.00$ (6.3.3.(4))
 $N_{Ed}/(X_z \cdot N_{Rk}/gM1) + k_{zy} \cdot M_{y,Ed,max}/(XLT \cdot M_{y,Rk}/gM1) + k_{zz} \cdot M_{z,Ed,max}/(M_{z,Rk}/gM1) = 0.44 < 1.00$ (6.3.3.(4))

Section OK !!!

STEEL DESIGN

CODE: *NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.*

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 5 Purlins

MEMBER: 102 Beam_102

POINT: 3

COORDINATE: x = 1.00 L =

4.00 m

LOADS:

Governing Load Case: 7 ULS /13/ 1*1.20 + 2*1.50

MATERIAL:

S235 (S235) $f_y = 235.00$ MPa

SECTION PARAMETERS: TELG 80x40x3

| | | | |
|-----------|----------------------------|---------------------------|-------------------------|
| h=8.0 cm | gM0=1.00 | gM1=1.00 | |
| b=4.0 cm | Ay=2.17 cm ² | Az=2.33 cm ² | Ax=4.53 cm ² |
| tw=0.3 cm | Iy=44.29 cm ⁴ | Iz=7.06 cm ⁴ | Ix=0.14 cm ⁴ |
| tf=0.3 cm | Wply=12.98 cm ³ | Wplz=4.45 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|-------------------------------|----------------------------------|----------------------------------|--------------------------------|
| N _{,Ed} = -0.29 kN | M _{y,Ed} = 1.96 kN*m | M _{z,Ed} = -0.27 kN*m | V _{y,Ed} = 0.36 kN |
| N _{t,Rd} = 106.38 kN | M _{y,pl,Rd} = 3.05 kN*m | M _{z,pl,Rd} = 1.05 kN*m | V _{y,T,Rd} = 29.39 kN |
| | M _{y,c,Rd} = 3.05 kN*m | M _{z,c,Rd} = 1.05 kN*m | V _{z,Ed} = 2.39 kN |
| | M _{N,y,Rd} = 3.05 kN*m | M _{N,z,Rd} = 1.05 kN*m | V _{z,T,Rd} = 31.68 kN |
| | | | T _{t,Ed} = 0.00 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About y axis:



About z axis:

VERIFICATION FORMULAS:

Section strength check:

$$N_{,Ed}/N_{t,Rd} = 0.00 < 1.00 \quad (6.2.3.(1))$$

$$M_{y,Ed}/M_{N,y,Rd} = 0.64 < 1.00 \quad (6.2.9.1.(2))$$

$$M_{z,Ed}/M_{N,z,Rd} = 0.26 < 1.00 \quad (6.2.9.1.(2))$$

$$(M_{y,Ed}/M_{N,y,Rd})^{1.00} + (M_{z,Ed}/M_{N,z,Rd})^{1.00} = 0.90 < 1.00 \quad (6.2.9.1.(6))$$

$$V_{y,Ed}/V_{y,c,Rd} = 0.01 < 1.00 \quad (6.2.6.(1))$$

$$V_{z,Ed}/V_{z,c,Rd} = 0.08 < 1.00 \quad (6.2.6.(1))$$

Section OK !!!

STEEL DESIGN

CODE: NEN-EN 1993-1:2006/NB:2016/A1:2014, Eurocode 3: Design of steel structures.

ANALYSIS TYPE: Code Group Verification

CODE GROUP: 6 Gutters

MEMBER: 126 Beam_126

POINT: 1

COORDINATE: x = 0.00 L =

0.00 m

LOADS:

Governing Load Case: 7 ULS /13/ 1*1.20 + 2*1.50

MATERIAL:

S235 (S235) $f_y = 235.00$ MPa

SECTION PARAMETERS: TELG 100x65x3

| | | | |
|-----------|----------------------------|----------------------------|-------------------------|
| h=14.6 cm | gM0=1.00 | gM1=1.00 | |
| b=6.5 cm | Ay=4.11 cm ² | Az=3.77 cm ² | Ax=8.77 cm ² |
| tw=0.3 cm | Iy=205.75 cm ⁴ | Iz=54.43 cm ⁴ | Ix=0.28 cm ⁴ |
| tf=0.3 cm | Wply=39.37 cm ³ | Wplz=20.27 cm ³ | |

INTERNAL FORCES AND CAPACITIES:

| | | | |
|-------------------------------|----------------------------------|----------------------------------|--------------------------------|
| N _{,Ed} = 0.21 kN | M _{y,Ed} = -0.01 kN*m | M _{z,Ed} = 3.05 kN*m | V _{y,Ed} = 3.65 kN |
| N _{c,Rd} = 206.00 kN | M _{y,pl,Rd} = 9.25 kN*m | M _{z,pl,Rd} = 4.76 kN*m | V _{y,T,Rd} = 55.75 kN |
| N _{b,Rd} = 206.00 kN | M _{y,c,Rd} = 9.25 kN*m | M _{z,c,Rd} = 4.76 kN*m | V _{z,Ed} = 0.00 kN |
| | MN _{,y,Rd} = 9.25 kN*m | MN _{,z,Rd} = 4.76 kN*m | V _{z,T,Rd} = 51.12 kN |
| | | | T _{t,Ed} = 0.00 kN*m |
| | | | Class of section = 1 |



LATERAL BUCKLING PARAMETERS:

BUCKLING PARAMETERS:



About y axis:



About z axis:

VERIFICATION FORMULAS:

Section strength check:

$$N_{,Ed}/N_{c,Rd} = 0.00 < 1.00 \quad (6.2.4.(1))$$

$$M_{y,Ed}/M_{N,y,Rd} = 0.00 < 1.00 \quad (6.2.9.1.(2))$$

$$M_{z,Ed}/M_{N,z,Rd} = 0.64 < 1.00 \quad (6.2.9.1.(2))$$

$$(M_{y,Ed}/M_{N,y,Rd})^{1.00} + (M_{z,Ed}/M_{N,z,Rd})^{1.00} = 0.64 < 1.00 \quad (6.2.9.1.(6))$$

$$V_{y,Ed}/V_{y,c,Rd} = 0.07 < 1.00 \quad (6.2.6.(1))$$

$$V_{z,Ed}/V_{z,c,Rd} = 0.00 < 1.00 \quad (6.2.6.(1))$$

Section OK !!!